

## Turbofan Noise Generation Volume 2: Computer Programs

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VOLUME 2: COMPUTER PROGRAMS

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## SUMMARY OF VOLUME 2

The computations for three different noise mechanisms - mean rotor wake, inlet turbulence, and rotor wake turbulence - described in Volume 1 of this report are coded as three separate computer program "packages." This arrangement was deemed reasonable because of differences in the required input data (e.g., rotor vs stator geometries), because of interest in the role of each separate noise mechanism, and for economy of execution during parametric studies. The computer codes are described by means of block diagrams, tables of data and variables, and example program executions. Reference to Volume 1 will be made via equation or figure number. FORTRAN listings of the programs appear in the appendix to Volume 2.

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## CHAPTER 1

### MEAN ROTOR WAKE PROGRAM

The computer program described in Fig. 1\* computes the sound power of each propagating mode for the first three harmonics of the blade passage frequency. The data required to run the program and the program results are described in Table 1.\* Important FORTRAN variables used in the program are given in Table 2. Function subroutines utilized in the program are described in Table 3.

The terminal output from a sample execution of the Mean Rotor Wake Program is shown in Table 4 for the rotor/stator data provided by NASA Lewis. The mean flow velocity entering the stator is specified from measured data. The pressure amplitude and sound power of each mode for each harmonic number of the blade passage frequency are listed. Note that for a propagating mode  $(m, n)$  at harmonic  $s$ , another mode  $(-m, n)$  of equal amplitude propagates with frequency  $-s$ . Thus the total sound power for the mode shape  $(|m|, n)$  at frequency  $|s|x$  (blade passage frequency) is the sum of the two components.

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\*Note: Because of the number and complexity of the figures and tables, they have been collected at the end of each section of this volume. The 9 text figures and 12 tables appear before the appendix.

## CHAPTER 2

### TURBULENCE PROGRAMS

The calculations for two types of turbulence noise are considerably more time-consuming than for the tones of the mean-wake interaction because 1) all modes that are not cut off by the duct may be excited, i.e., there is no selection rule, as is the case for the mean-wake interaction, and 2) the noise is broadband rather than tonal, requiring the sound power at many frequencies to be calculated. For these reasons, the turbulence programs are each broken into two subsections. The method used is, first, to calculate and store, for a given number of blade radii, the pressure distributions across the rotor blades or stator vanes at a small number of frequencies over the range of interest. The power spectral density is essentially a spatial integral containing the pressure distribution and acoustic mode shape as factors in the integrand. The pressure distributions are slowly varying functions of frequency and duct radius when compared with the acoustic mode shapes. Thus it is reasonable to interpolate the pressure distribution for a specific frequency and radius from a look-up table of stored pressure values. All other variables that change with radius (or frequency) are calculated explicitly for that given radius (frequency). In this manner, convergence of the radial integration is improved by using more integration steps than there are stored pressure values. The pressure distributions are stored in binary form in a disc file for later use so that, for example, turbulence parameter values may be varied without recomputing the pressures.

#### 2.1 Inlet Turbulence Program

The pressure distributions across the rotor blades are computed and stored as described in Fig. 2. The sound power calculation is diagrammed in Fig. 3. Input and output data for the programs are listed in Table 5. Additional program variables of possible interest to the user are given in Table 6.

Output from sample executions of the two program sections is shown in Tables 7 and 8. The input data relating to rotor geometry and performance are first entered as listed in Table 7. The pressure distributions are computed (as evidenced by the error code returned from LEQTIC; see Table 3), and the data are stored on a disc. The power spectral density for all propagating modes at a frequency of 15 times shaft rate (blade passage frequency in this 15-blade fan) is then computed, and the results are given in Table 8.

## 2.2 Rotor Wake Turbulence Program

The two-stage method of calculation described above is repeated for the Rotor Wake Turbulence problem. The calculation of pressure distributions across the stator vanes proceeds as shown in Fig. 4. The sound power calculation is explained in Fig. 5. Input and output data for the programs are listed in Table 9. Additional program variables are given in Table 10.

The output from sample program executions is shown in Tables 11 and 12. The mean flow into the stator may be specified as for the Mean Wake case. (Note that the print-out shown in Table 12 has been stripped of all messages other than the power spectral density per mode to minimize the amount of paper delivered for high frequencies (many modes). The standard program version would contain diagnostic messages, cut-off ratios, etc., as for Table 8.

## CHAPTER 3

### EXECUTION PARAMETERS AND PROGRAM LIMITATIONS

#### A. General Remarks

1. Specifying blade or vane geometries: Geometrical data are stored in matrix VGEOM. The number of radial positions at which data may be specified (NDAT) is presently limited to 10 by DIMENSION statements. This limitation may be lifted by increasing the size of VGEOM in all main and subprograms. The geometrical data are specified by proceeding radially from hub to tip, and must include these two end points. These data are linearly interpolated for integration stations between the data points.

2. Specifying mean flow distributions: Variable IVOR is a switch controlling whether a free vortex distribution (IVOR=0) or input data (IVOR=1) are used in stator calculations. Input data are stored in matrix VELOCV. The number of radial positions at which data are specified (NVELO) is presently limited to 10. This limitation may be lifted by increasing the size of VELOCV in all main and subprograms. The velocity data are specified by proceeding radially from hub to tip and must include these two endpoints. These data are also linearly interpolated for intermediate points in the radial integration.

3. Specifying Bessel function accuracies: The absolute accuracies for all Bessel function calculations (EB) and root convergence (EC) have been left as input parameters. Values of 0.001 and 0.0001, respectively, have been sufficient for these calculations.

4. Specifying the number of chordwise integration points: The number of chordwise integration points (NCHORD) is an input variable. DIMENSION statements currently limit the value of NCHORD to 20 in all programs. A value of 8 has yielded sufficient accuracy in the cases checked to date. Execution time increases radically for increases in NCHORD, so its value should be minimized. For cases where the acoustic wavelength is considerably less than the blade or stator chord, it may be necessary to increase NCHORD beyond 8. If NCHORD must be increased beyond 20, the following array sizes must be inspected and/or increased: CASCET, PHASE, DELTAP, F, A, WA, and B.

5. Specifying the number of radial integration points:  
The number of radial integration points (NRAD in Mean Wake,  
or NRADNU in the turbulence programs) is an input variable.  
The value must be large enough to achieve convergence of the  
result, yet small enough to minimize program execution time.  
A value of 7 has yielded adequate accuracy ( $\pm 1$  dB) for the  
acoustic power levels in cases checked to date. The value  
of 20 must not be exceeded without inspecting and/or  
increasing the sizes of arrays PSIST0, BJ, RR, RRNU, and  
ASCET.

## B. Turbulence Programs

1. Specifying the number of radial positions for pressure calculations: Both turbulence programs compute and store pressure distributions at a number (NRAD) of radial positions. Acoustic calculations are later performed by using NRADNU (>NRAD) integration points. This arrangement minimizes the execution time needed for pressure calculations while maintaining good accuracy in the radial integral. NRAD values of 5 have been used for the test cases cited here. NRAD may not be increased beyond 20 without violating DIMENSION statements, as discussed in Sec. A.5.

2. Range of Mode Number m: The turbulence programs that compute power spectral densities contain a summation of autocorrelation functions that vary with mode number m. If the annular duct/turbofan arrangement were to allow propagation of modes with mode number  $|m|$  greater than 49 at a given frequency, then program execution would be terminated with an error message. This range may be increased by increasing the size of arrays ISUMTO and SUMTOT and by changing the decision value in the associated IF statement.

3. Selection of frequency values for data storage: The turbulence programs compute and store pressure distributions for a range of frequencies for later interpolation. The most useful frequencies to calculate in the subject spectrum of, for example, from 1 to 3 times the blade passage frequency (BPF), are probably the first, second, and third harmonics of BPF. This range is straightforwardly specified for the wake turbulence program. An important qualification to this procedure must be invoked for inflow turbulence, as explained below.

The sound power calculations for the inflow turbulence routine require pressure distribution data for frequencies up to an equivalent frequency

$$(\omega^*/\Omega) = (\omega/\Omega)_{\max} + |m_{\max}| + m_{\text{sum}},$$

where  $(\omega/\Omega)_{\max}$  is the highest frequency of interest,  $m_{\max}$  is the largest value of  $m$  which can propagate at frequency  $(\omega/\Omega)$ , and  $m_{\text{sum}} = -|m_{\max}| + (\ell B)$  for some integer  $\ell$  such that  $0 \leq m_{\text{sum}} \leq B-1$ , for  $B$ =number of rotor blades. Thus, before computing the pressure distribution, the user must know what modes can propagate for the turbofan under discussion. The utility program MAPIN/MAPPER (see appendix) will yield the propagating modes for a given geometry, frequency, and turbofan speed. As an example, suppose that the turbulence noise spectrum between BPF and 3BPF is desired for NASA Rotor 55 with the operating conditions: Number of blades = 15,  $M_t = 0.508$ ,  $M = 0.323$ , and  $\sigma_r = 0.484$ . Pressure data will be needed from the lowest frequency of interest ( $\omega/\Omega = \text{BPF} = 15$ ) to the highest equivalent frequency  $(\omega^*/\Omega)$ . Program MAPIN/MAPPER reveals that  $|m_{\max}| = 21$  for  $(\omega/\Omega) = 3\text{BPF} = 45$ . Thus,

$$(\omega^*/\Omega) = (\omega/\Omega)_{\max} + |m_{\max}| + m_{\text{sum}}$$

$$(\omega^*/\Omega) = 45 + 21 + 9 = 75,$$

$$\text{where } m_{\text{sum}} = -21 + (2 \cdot 15) = 9.$$

In the example,  $(\omega^*/\Omega)$  conveniently falls at the fifth multiple of blade passage frequency (5BPF) or  $\omega/\Omega = 75$ . The frequency range for pressure distribution calculations is then from  $(\omega/\Omega) = 15$  to  $(\omega/\Omega) = 75$  in steps of  $(\omega/\Omega) = 15$ . The results of calculations for that case are shown in Table 7. If programs INSRCH/INTURB were to be executed without pressure data of sufficiently high equivalent frequency, the program execution would be terminated with an error message.

4. DIMENSION of storage matrix CASCET: Pressure distributions are stored on the disc in matrix CASCET. It is desirable to keep this matrix as small as possible to minimize core and disc file requirement... The DIMENSION of CASCET should therefore be adjusted as follows to suit the data: DIMENSION CASCET (NCHORD, NRAD, NBLADE, PRANGE), where NCHORD = number of chordwise integration points, NRAD = number of radial positions for pressure calculations, NBLADE = number of rotor blades, or, for the Rotor Wake Turbulence Program, use NVANE = number of stator vanes. PRANGE = number of frequencies for pressure calculations.

## FIGURES

Calculate the sound power of each propagating mode for the first 3 harmonics of the blade passage frequency.

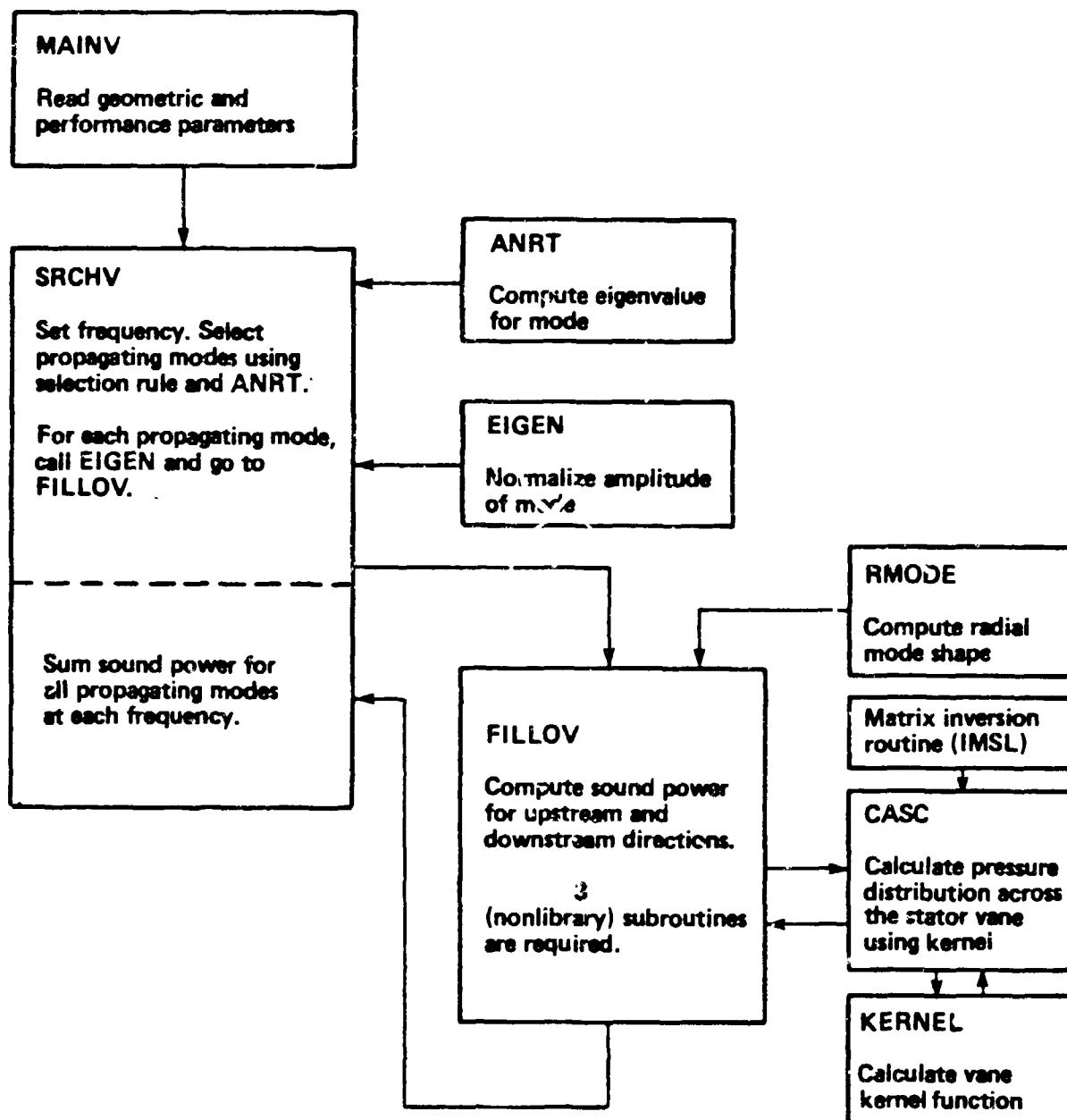


Figure 1. Block Diagram of Mean Rotor Wake Program

A. Calculate pressure distributions across the rotor blades and store data on the disk.

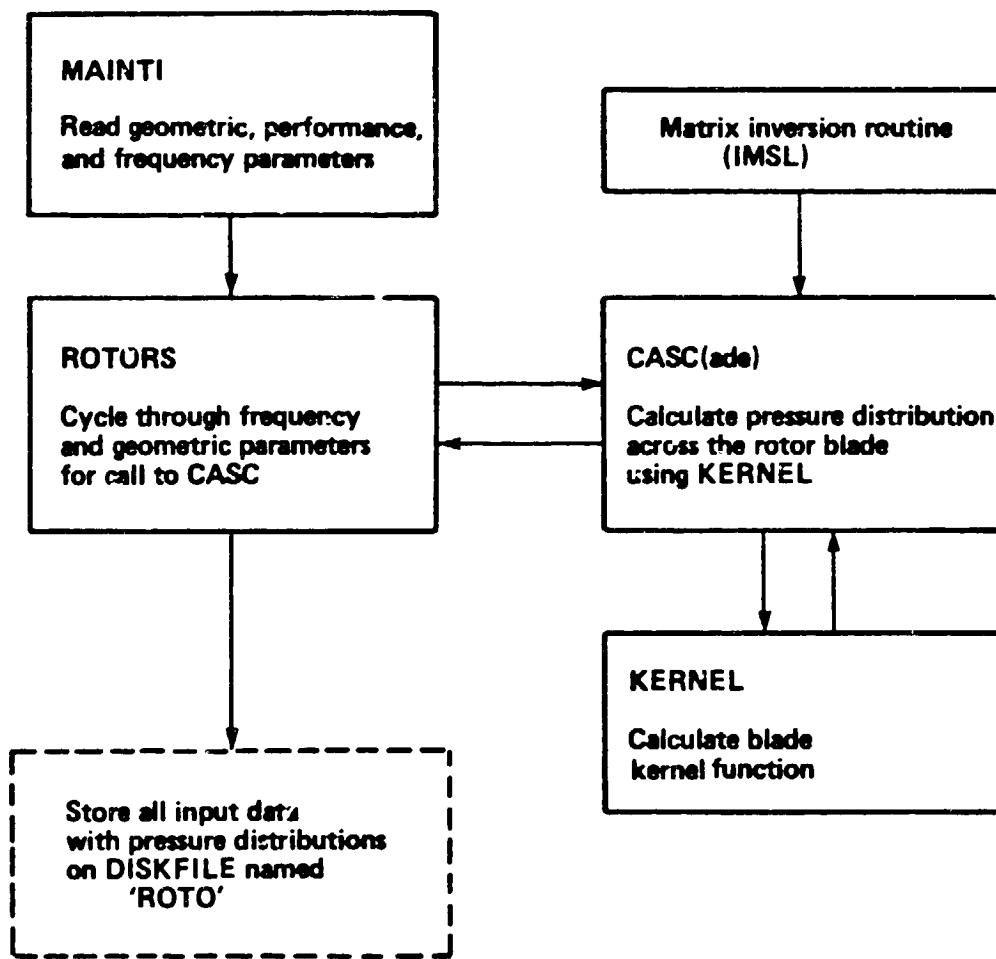


Figure 2. Block Diagram of Inlet Turbulence Program;  
Part A: Data Storage

- B. Calculate the power spectral density of each propagating mode at a given frequency and the total PSD for all modes.

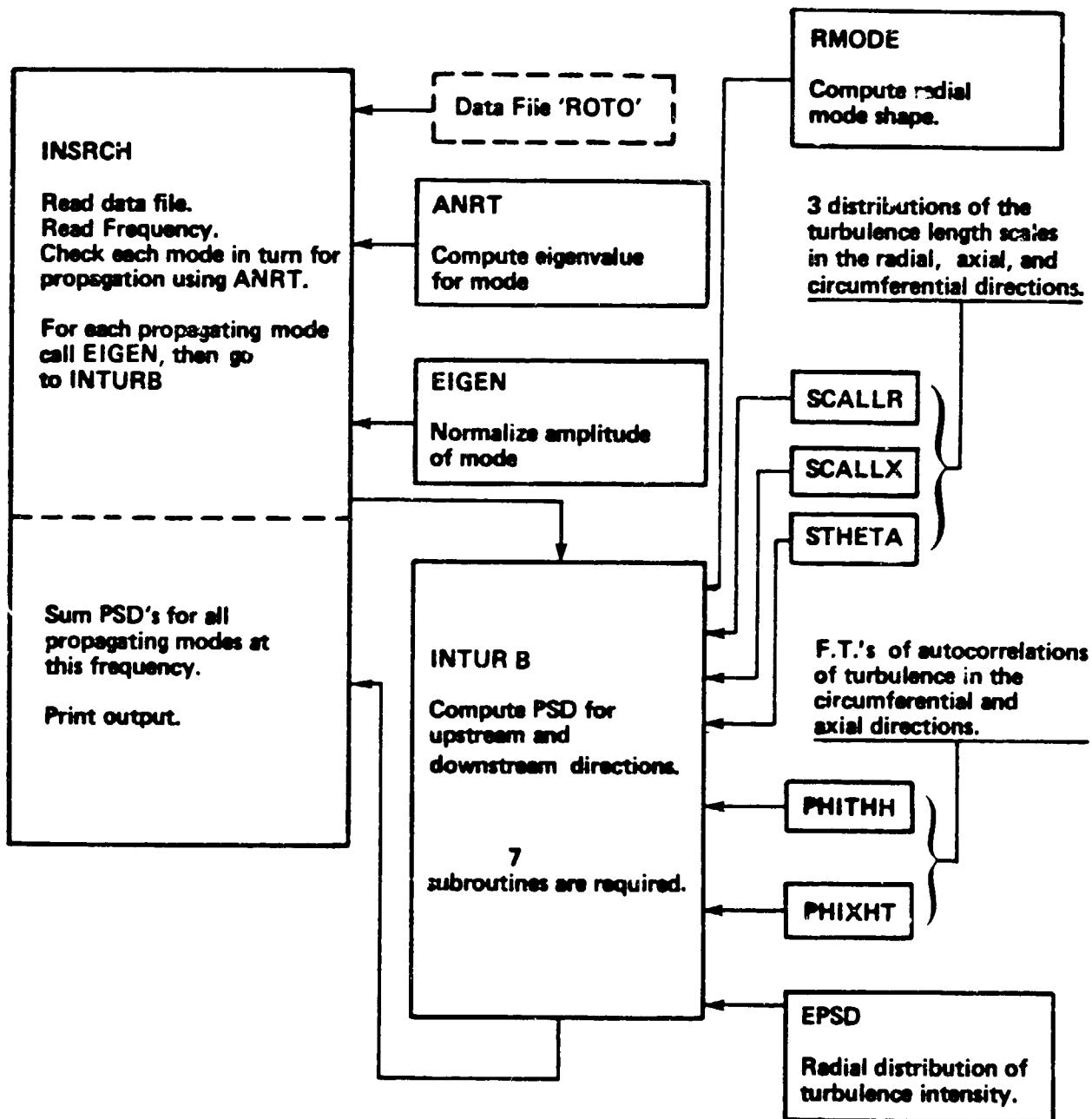


Figure 3. Block Diagram of Inlet Turbulence Program;  
Part B: Noise Calculation

A. Calculate pressure distributions across the stator vanes and store data on the disk.

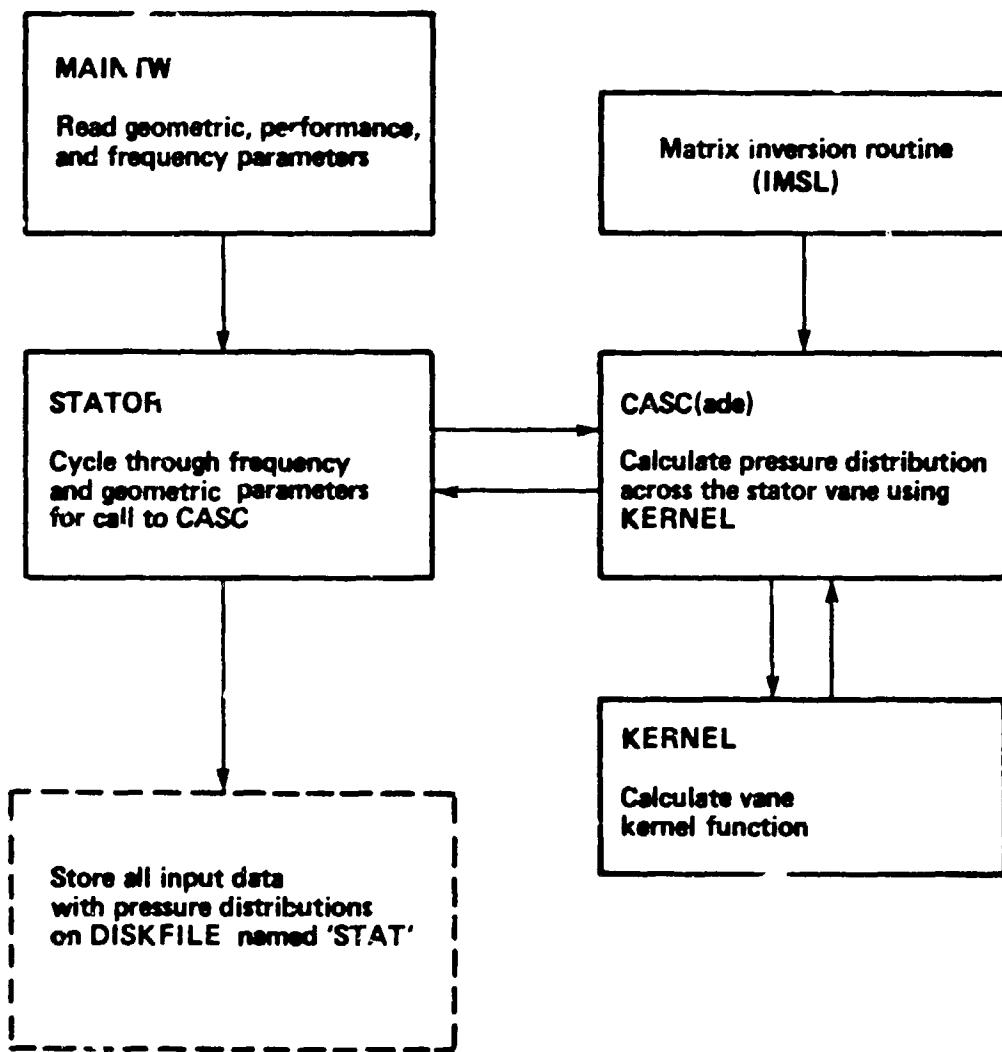


Figure 4. Block Diagram of Rotor Wake Turbulence Program; Part A: Data Storage

B. Calculate the power spectral density of each propagating mode at a given frequency and the total PSD for all modes.

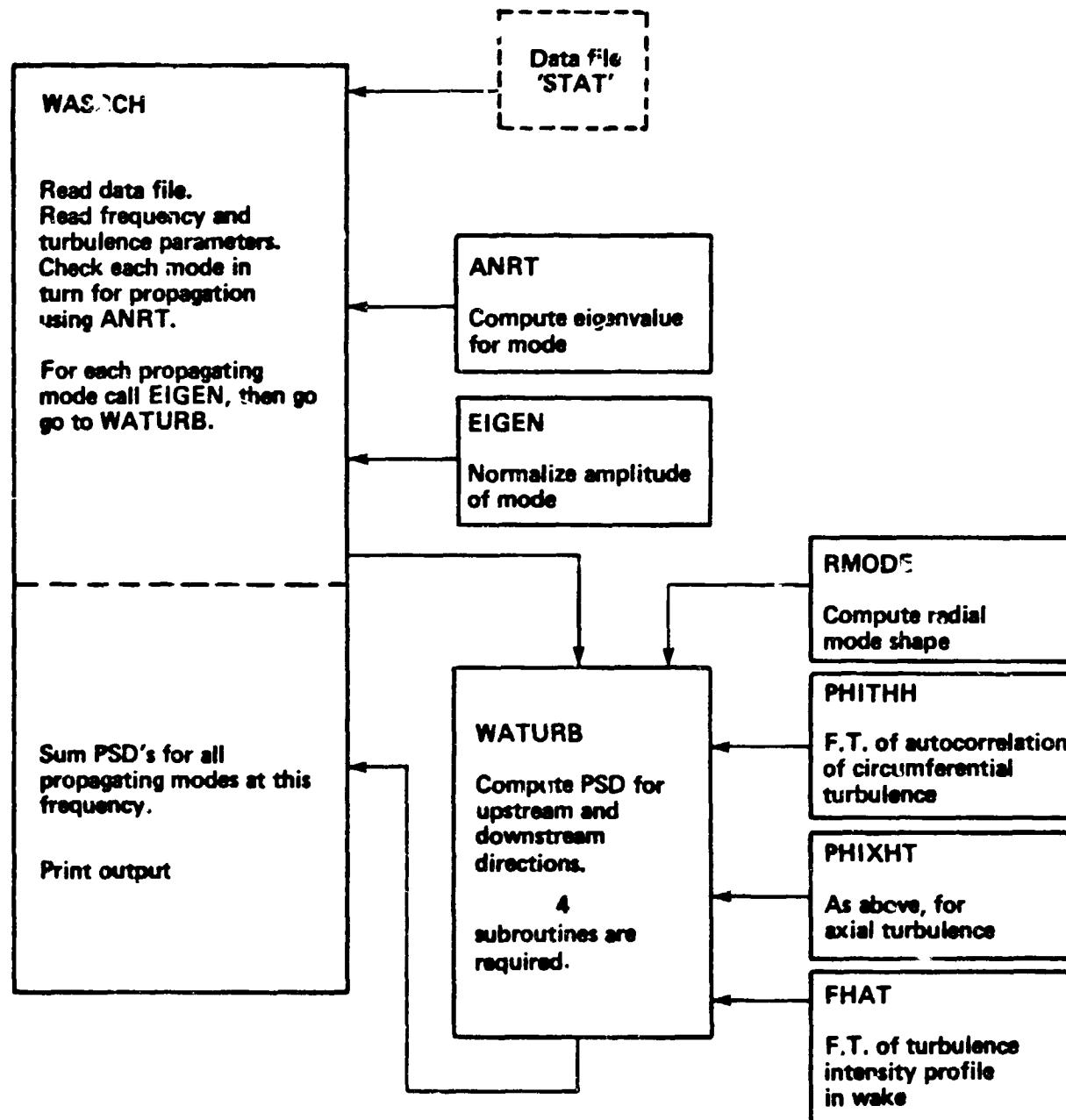


Figure 5. Block Diagram of Rotor Wake Turbulence Program;  
Part B: Noise Calculation

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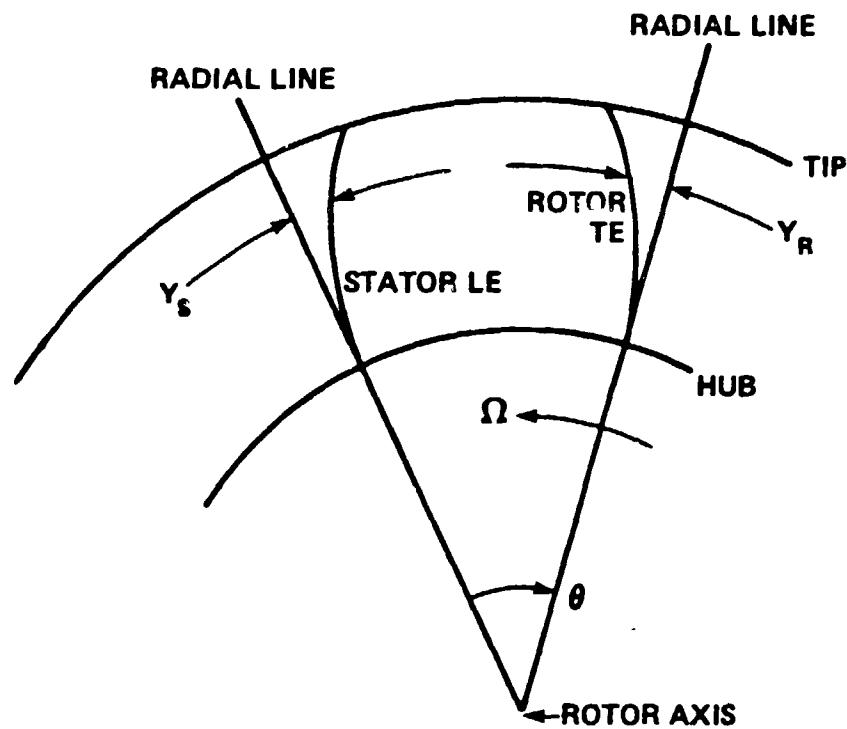


Figure 6. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Down the Turbofan X Axis, in Stator-Fixed Coordinates

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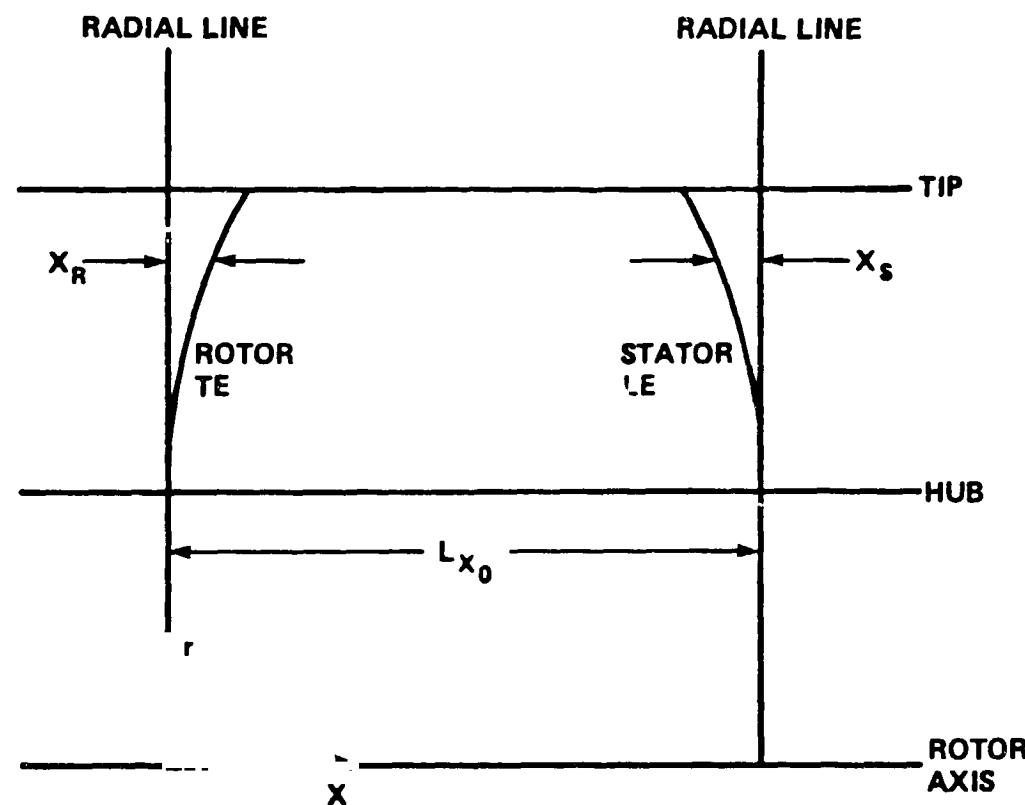


Figure 7. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Perpendicular to the Rotor Axis

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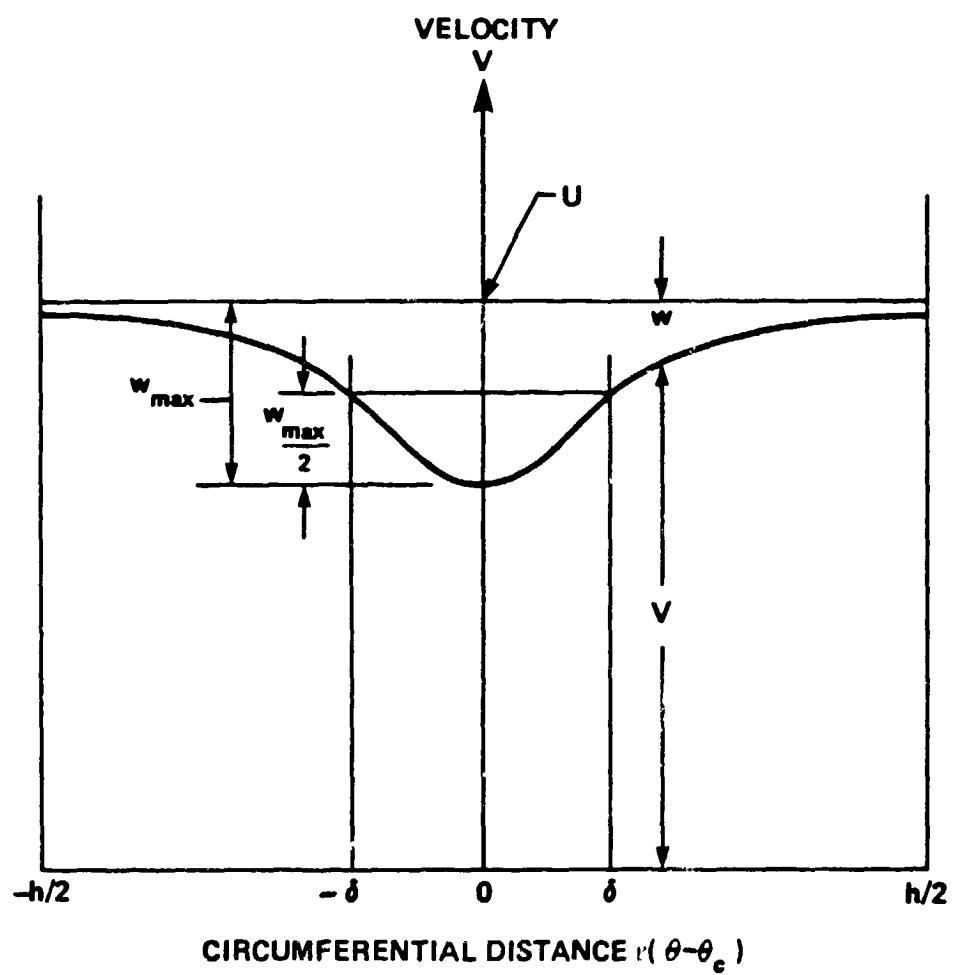


Figure 8. Typical Wake Profile

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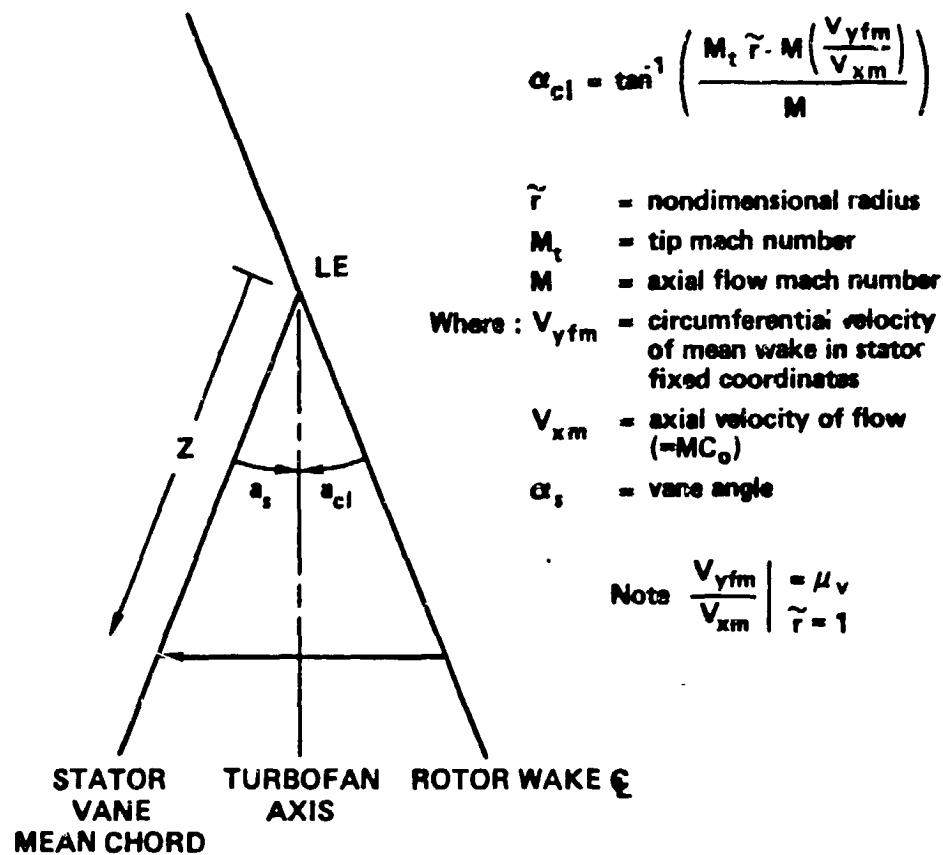


Figure 9. Schematic Diagram of the Stator Vane Mean Chord at the Instant When the Wake Centerline Intersects the Leading Edge

TABLES

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**TABLE 1. INPUT/OUTPUT DATA FOR THE MEAN ROTOR WAKE PROGRAM**

This program calculates the complex modal amplitude and the modal sound power generated by the interaction of the mean rotor wakes with the stator vanes. All input and output data are nondimensional. The input data consist of geometric, performance, and computational parameters.

**A. Geometric Data**

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	NBLADE	B	No. of rotor blades	Integer
2.	NVANE	V	No. of stator vanes	Integer
3.	SIGMAR	$\sigma_r$	Ratio of hub radius to duct radius	Floating Point
4.	SIGMAC	$\sigma_c$	Ratio of tip chord of stator vane to duct radius	Floating Point
5.	LXO	$d/r_{duct}$	Ratio of rotor-stator spacing to duct radius	Floating Point
6.			Vector of data for a number, NDAT (an integer variable) of stator vane radii	
a.	R	$\tilde{r}$	Nondimensional radius = $r/r_{duct}$	Floating Point
b.	C	$\tilde{c}$	Nondimensional vane chord = $c/c_{tip}$	Floating Point
c.	ALPHAS	$\alpha_s$	Vane angle (degrees)	Floating Point
d.	YS*	$\tilde{Y}_S$	Nonradial variation of stator leading edge = $Y_S/c_{tip}$	Floating Point
e.	YR*	$\tilde{Y}_R$	Nonradial variation of rotor trailing edge = $Y_R/c_{tip}$	Floating Point
f.	XS**	$\tilde{X}_S$	Axial variation of stator leading edge = $X_S/c_{tip}$	Floating Point
g.	XR**	$\tilde{X}_R$	Axial variation of rotor trailing edge = $X_R/c_{tip}$	Floating Point

\*See Figure 6

\*\*See Figure 7

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TABLE 1. (Cont.)

a. Performance Data

	FORTRAN NAME	SYMBOL	DESCRIPTION	FORTRAN VARIABLE TYPE
1.	MT	$M_t$	Mach number	Floating Point
2.	MA	M	Axial flow Mach number	Floating Point
3.	IVOR	-	Switch for rotor wake specification = 0 for free vortex distribution = 1 for specified input velocity distribution	Integer
4.			(for IVOR = 1) Vector of data for a number, NVELO, (an integer variable) of vane radii	
	R XVEL	$\tilde{r}$ $V_{yfm}$ $V_{xm}$	a. Nondimensional radius b. Ratio of circumferential velocity to axial flow velocity of the mean wake (See Fig. 9)	Floating Point Floating Point
5.	MUV	$\mu_v$	(for IVOR = 0) Ratio of circumfer- ential velocity at the duct radius to the axial flow velocity	Floating Point
6.	WWIDTH	$\delta/h$	Ratio of wake half-width to wake spacing (See Fig. 8)	Floating Point
7.	VELDEF	$W_{max}/U$	Ratio of maximum wake velocity deficit to the streamwise flow velocity (assumed constant with radius). (See Fig. 8)	Floating Point

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TABLE 1. (Cont.)

C. Computational Data

These data set the number of integration stations in the chordwise and spanwise directions (and, indirectly, the accuracy of the results). The required accuracy for the Bessel functions used in the mode shape and eigenvalue routines are also specified.

FORTRAN NAME	VARIABLE	FORTRAN VARIABLE TYPE
1. NRAD	No. of integration stations in the radial direction (odd number)	Integer
2. NCHORD	No. of integration stations in the chordwise direction (even number)	Integer
3. EB	Absolute accuracy of all Bessel function calculations	Floating Point
4. EC	Absolute accuracy of convergence to root of eigenvalue equation	Floating Point

Program Output

The output lists the complex nondimensional pressure amplitude for each propagating mode. The amplitude is nondimensionalized by the dynamic pressure of the mean axial flow  $\rho_0 U^2/2$ . Also given is the relative modal sound power level. To recover the conventional sound power level (dB re  $10^{-12}$  watt) add

$$10 \log_{10} \left[ \frac{\rho_0 c_0^3 M^* r_{duct}^2}{8 \cdot 10^{-12}} \right]$$

to the computed relative power. This step is required because all computations performed in the program are nondimensional with absolute values of  $\rho_0$ ,  $c_0$ , and  $r_{duct}$  unknown.

TABLE 2. IMPORTANT INTERNAL PROGRAM VARIABLES  
MEAN ROTOR WAKE PROGRAM

(Used in addition to the INPUT/OUTPUT variables.)

FORTAN NAME	SYMBOL	VARIABLE
AMN*	A <sub>m,n</sub>	
BMN*	B <sub>m,n</sub>	
ARG*	X <sub>m,n</sub>	Argument of the mode shape function $\psi$ ( $= \kappa_{m,n} r$ )
B*	b	Nondimensional vane semi-chord = $c/2c_{tip}$
BETASQ*	B <sup>2</sup>	1-M <sup>2</sup> , where M is the axial flow Mach no.
DELTAP	$\Delta \bar{p}$	Nondimensional complex pressure along vane chord
DELTAR*	$\Delta \tilde{r}$	Discrete radial interval for integration
GAMMA	$\Gamma$	Nondimensional wave number of the convected gust
GMNS*	$\tilde{\gamma}_{m,n,s}$	Nondimensional acoustic wavenumber for moving medium (See Eq. 88 of Vol. 1)
H1	$h_1$	Nondimensional stator vane spacing in direction parallel to vane (See Fig. B-1 of Vol. 1)
H2	$h_2$	Nondimensional stator vane spacing in direction perpendicular to vane (See Fig. B-1 of Vol. 1)
IER*, IERPS1	-	Error codes from Bessel function subroutines
IR*	-	Counter for integration stations in radial direction
IZ*	-	Counter for integration stations in chordwise direction
KMNS*	K <sub>m,n,s</sub>	Nondimensional acoustic wavenumber = $r_{duct} \cdot \tilde{\gamma}_{m,n,s}$ (See Eq. 88 of Vol. 1)

TABLE 2. (Cont.)

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KX	$k_x$	Nondimensional gustavenumber in the axial direction
MM*	m	Circumferential mode number
MR	$M_r$	Relative Mach number of mean wake (vector sum of rotational and axial components)
MYM	-	Relative circumferential Mach no. of mean wake at $\bar{r}$ .
NN*	n	Radial mode number
PMNS	-	Sum of terms comprising the radial integral
PSI*, OR PSISTO*	$\psi$	Nondimensional radial mode shape as a function of radius
QMNS	-	Sum of terms comprising the chordwise integral
R*	$\tilde{r}$	Nondimensional radius = $r/r_{duct}$
RELPRL	-	Relative modal sound power level at harmonic s
REPLWR, SPWR	-	Relative modal sound power at harmonic s
SB	sB	Product of harmonic number and no. of blades
SS	s	Harmonic number (=1,2,3) multiple of the rotor blade passage frequency
WH	$\hat{w}$	Complex nondimensional amplitude of gust velocity impinging on stator vane
WHTC	-	Weighting factor for Simpson Integration method used in chordwise integral
XMN*	$k_{m,n} r_{duct}$	Nondimensional root of duct eigenvalue equation (See Eq. 6 of Vol. 1)

\*These variables are also used in the inlet and wake turbulence programs, but are listed here only.

TABLE 3. UTILITY SUBROUTINES

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## A. Subroutines common to the Mean Wake, Inlet, and Wake Turbulence programs.

1. ANRT (ANnular Root), ANFU (ANnular FUnction), ISIGN  
Programs find the roots  $\kappa_{m,n}$  of the boundary value equation  
for the annular duct:

$$J_m'(\kappa_{m,n} r_{duct}) Y_m'(\kappa_{m,n} r_{hub}) - J_m'(\kappa_{m,n} r_{hub}) Y_m'(\kappa_{m,n} r_{duct}) = 0$$

2. FLSJ, BESY (Bessel functions of the first [J] and the second [Y] kind)

BESJ computes the mth order Bessel function of the first kind,  $J_m(x)$ .

BESY computes the mth order Bessel function of the second kind,  $Y_m(x)$ .

An error code is returned along with each answer. The error code is:

- ERR = 0 No error (answer is correct to given accuracy)
- 1 m was negative (must be  $\geq 0$ )
- 2 Argument was negative (must be  $\geq 0$ )
- 3 Required accuracy not obtained
- 4 Range of n compared to the argument was not correct (see program listing).

## 3. EIGEN

The program normalizes the weighting factors  $A_{m,n}$  and  $B_{m,n}$  used in the mode function.

$$\psi = A_{m,n} J_m + B_{m,n} Y_m.$$

The orthogonality condition is

$$\int_A \psi_{i,j} \psi_{m,n}^* dA = \begin{cases} \Gamma_{m,n} & \text{if } i = m \text{ and } j = n \\ 0 & \text{otherwise} \end{cases}$$

The normalizing condition used is that

$$\tilde{\Gamma}_{m,n} \equiv \frac{\Gamma_{m,n}}{\pi(r_{duct}^2 - r_{hub}^2)} = 1 \text{ (non-dimensional).}$$

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TABLE 3. (Cont.)

4. RMODE

Program computes the radial mode shape  $\psi$  for the  $m$ ,  $n$ th mode of the annular duct. (See Eq. 4 of Vol. 1)

5. KERNEL

Program computes the kernel for the Green's function formulation of the cascade routine. (See Eqs. B-25 and B-26 of Vol. 1)  
Used in conjunction with PRES or CASC.

B. Subroutine used specifically for the Mean Wake Routine

1. PRES (PRESSure distribution)

The program specifies the complex pressure distribution across the stator vane chord as produced by a velocity gust. The input parameters include the gust wavenumber, the wake velocity, and the stator vane spacings.

C. Subroutines used specifically for the Inlet Turbulence Routine

1. SCALLX (SCALE Length, X direction)

Program yields the turbulence length scale in the axial direction as a function of radial position. The routine is actually a program input whereby a particular turbulence distribution is loaded.

2. SCALLR (SCALE Length, Radial direction)

Program yields the turbulence length scale in the radial direction as a function of radial position. The routine is an input parameter.

3. STHETA (Scale length, THETA direction)

Program yields the turbulence length scale in the circumferential direction as a function of radial position. The routine is an input parameter.

4. EPSD ( $\epsilon_D$ )

Program yields the inlet RMS turbulence intensity as a function of radial position. The routine is an input parameter.

5. PHITHH ( $\hat{\phi}_\theta$ )

The program computes the Fourier transform of the correlation function in the circumferential direction. This transform is usually a fairly simple analytic function such as an exponential.

TABLE 3. (Cont.)

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6. PHIXHT ( $\hat{\phi}_x$ )

The program computes the Fourier transform of the correlation function in the axial direction.

## D. Subroutines used for the Inlet and Wake Turbulence Routines

## 1. CASC (CASCaDe function)

The program calculates the complex pressure distribution across a blade chord as produced by a velocity gust. The input parameters include the gust wavenumber, the wake velocity, and the blade spacings. This program is a version of PRES (listed above) specialized for use with the extended range of arguments in the turbulence routines.

## E. Subroutine used specifically for the Wake Turbulence Routine

1. FHAT ( $\hat{f}$ )

The program computes the Fourier transform of the modulating function for the turbulent wake. The transform is usually a simple analytic function depending on the turbulence model in use.

## F. IMSL Library Subroutine called by Subroutine KERNEL

IMSL Library routine LEQTIC is called by KERNEL to solve a set of simultaneous equations. The documentation provided by IMSL follows on the next three pages.

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TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQTIC.

IMSL ROUTINE NAME	- LEQTIC																		
PURPOSE	- LINEAR EQUATION SOLUTION - COMPLEX MATRIX - SPACE ECONOMIZER SOLUTION																		
USAGE	- CALL LEQTIC (A,N,IA,B,M,IB,IJOB,WA,IER)																		
ARGUMENTS	<table border="0"> <tr> <td>A</td><td>- INPUT COMPLEX N BY N MATRIX CONTAINING THE COMPLEX COEFFICIENTS OF THE EQUATION AX = B. ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF A ROWWISE PERMUTATION OF THE INPUT MATRIX A.</td></tr> <tr> <td>N</td><td>- ORDER OF MATRIX A. (INPUT)</td></tr> <tr> <td>IA</td><td>- ROW DIMENSION OF MATRIX A EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)</td></tr> <tr> <td>B</td><td>- INPUT COMPLEX N BY M MATRIX CONTAINING THE 1 COMPLEX VALUED RIGHT HAND SIDES OF THE EQUATION AX = B. ON OUTPUT, THE SOLUTION MATRIX X REPLACES B. IF IJOB=1, B IS NOT USED.</td></tr> <tr> <td>M</td><td>- NUMBER OF RIGHT HAND SIDES (COLUMNS IN B). (INPUT)</td></tr> <tr> <td>IB</td><td>- ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)</td></tr> <tr> <td>IJOB</td><td>- INPUT OPTION PARAMETER. IJOB=I IMPLIES WHEN I=0, FACTOR THE MATRIX AND SOLVE THE EQUATION AX=B. I=1, FACTOR THE MATRIX A. I=2, SOLVE THE EQUATION AX=B. THIS OPTION IMPLIES THAT LEQTIC HAS ALREADY BEEN CALLED USING IJOB=0 OR 1 SO THAT THE MATRIX HAS ALREADY BEEN FACTORED. IN THIS CASE OUTPUT MATRIX A MUST HAVE BEEN SAVED FOR REUSE IN THE CALL TO LEQTIC.</td></tr> <tr> <td>WA</td><td>- WORK AREA OF LENGTH N CONTAINING THE PIVOT INDICES.</td></tr> <tr> <td>IER</td><td>- ERROR PARAMETER. (OUTPUT) TERMINAL ERROR IER=129 INDICATES THAT MATRIX A IS ALGORITHMICALLY SINGULAR. (SEE THE CHAPTER L PRELUDE.)</td></tr> </table>	A	- INPUT COMPLEX N BY N MATRIX CONTAINING THE COMPLEX COEFFICIENTS OF THE EQUATION AX = B. ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF A ROWWISE PERMUTATION OF THE INPUT MATRIX A.	N	- ORDER OF MATRIX A. (INPUT)	IA	- ROW DIMENSION OF MATRIX A EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)	B	- INPUT COMPLEX N BY M MATRIX CONTAINING THE 1 COMPLEX VALUED RIGHT HAND SIDES OF THE EQUATION AX = B. ON OUTPUT, THE SOLUTION MATRIX X REPLACES B. IF IJOB=1, B IS NOT USED.	M	- NUMBER OF RIGHT HAND SIDES (COLUMNS IN B). (INPUT)	IB	- ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)	IJOB	- INPUT OPTION PARAMETER. IJOB=I IMPLIES WHEN I=0, FACTOR THE MATRIX AND SOLVE THE EQUATION AX=B. I=1, FACTOR THE MATRIX A. I=2, SOLVE THE EQUATION AX=B. THIS OPTION IMPLIES THAT LEQTIC HAS ALREADY BEEN CALLED USING IJOB=0 OR 1 SO THAT THE MATRIX HAS ALREADY BEEN FACTORED. IN THIS CASE OUTPUT MATRIX A MUST HAVE BEEN SAVED FOR REUSE IN THE CALL TO LEQTIC.	WA	- WORK AREA OF LENGTH N CONTAINING THE PIVOT INDICES.	IER	- ERROR PARAMETER. (OUTPUT) TERMINAL ERROR IER=129 INDICATES THAT MATRIX A IS ALGORITHMICALLY SINGULAR. (SEE THE CHAPTER L PRELUDE.)
A	- INPUT COMPLEX N BY N MATRIX CONTAINING THE COMPLEX COEFFICIENTS OF THE EQUATION AX = B. ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF A ROWWISE PERMUTATION OF THE INPUT MATRIX A.																		
N	- ORDER OF MATRIX A. (INPUT)																		
IA	- ROW DIMENSION OF MATRIX A EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)																		
B	- INPUT COMPLEX N BY M MATRIX CONTAINING THE 1 COMPLEX VALUED RIGHT HAND SIDES OF THE EQUATION AX = B. ON OUTPUT, THE SOLUTION MATRIX X REPLACES B. IF IJOB=1, B IS NOT USED.																		
M	- NUMBER OF RIGHT HAND SIDES (COLUMNS IN B). (INPUT)																		
IB	- ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED IN THE DIMENSION STATEMENT IN THE CALLING PROGRAM. (INPUT)																		
IJOB	- INPUT OPTION PARAMETER. IJOB=I IMPLIES WHEN I=0, FACTOR THE MATRIX AND SOLVE THE EQUATION AX=B. I=1, FACTOR THE MATRIX A. I=2, SOLVE THE EQUATION AX=B. THIS OPTION IMPLIES THAT LEQTIC HAS ALREADY BEEN CALLED USING IJOB=0 OR 1 SO THAT THE MATRIX HAS ALREADY BEEN FACTORED. IN THIS CASE OUTPUT MATRIX A MUST HAVE BEEN SAVED FOR REUSE IN THE CALL TO LEQTIC.																		
WA	- WORK AREA OF LENGTH N CONTAINING THE PIVOT INDICES.																		
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PRECISION/HARDWARE	- SINGLE AND DOUBLE/H32 - SINGLE/H36,H48,H60																		
REQD. IMSL ROUTINES	- UERTST,UGETIO																		
NOTATION	- INFORMATION ON SPECIAL NOTATION AND CONVENTIONS IS AVAILABLE IN THE MANUAL INTRODUCTION OR THROUGH IMSL RCUTINE UHELP																		
REMARKS	<ol style="list-style-type: none"> <li>1. WHEN IJOB=1, ARGUMENTS B, M AND IB ARE NOT USED BY LEQTIC.</li> <li>2. INPUT MATRIX A IS DESTROYED WHEN IJOB=0 OR 1. WHEN IJOB=0 OR 2, B IS REPLACED WITH THE SOLUTION X.</li> </ol>																		

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TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQTIC.

3. LEQTIC CAN BE USED TO COMPUTE THE INVERSE OF A COMPLEX MATRIX. THIS IS DONE BY CALLING LEQTIC WITH M=N, B=THE N BY N IDENTITY MATRIX AND IJOB=0. WHEN N IS LARGE, IT MAY BE MORE PRACTICAL TO COMPUTE THE INVERSE A COLUMN AT A TIME. TO DO THIS, FIRST CALL LEQTIC WITH IJOB=1 TO FACTOR A. MAKE SUCCEEDING CALLS WITH M=1, B =A COLUMN OF THE IDENTITY MATRIX AND IJOB=2. B WILL BE REPLACED BY THE CORRESPONDING COLUMN OF A INVERSE.
4. THE DETERMINANT OF A CAN BE COMPUTED AFTER LEQTIC HAS BEEN CALLED AS FOLLOWS

```
DET = (1.0,0.0)
DO 5 I = 1,N
  IPVT = WA(I)
  IF (IPVT .NE. I) DET = -DET
  DET = DET*A(I,I)
5 CONTINUE
```

Algorithm

For a given N by N complex matrix A and an N by M complex matrix B, LEQTIC computes an LU decomposition of a rowwise permutation of A and solves the system of equations AX=B. Row equilibration and partial pivoting are used.

See reference:

Forsythe, George and Moler, Cleve B., Computer Solution of Linear Algebraic Systems, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1967.

Example

This example shows how-to solve a system of 3 equations in 3 unknowns using LEQTIC.

The equations are

$$\begin{aligned}(1.+i3.)X(1) + (2.5-i3.5)X(2) + (1.+i)X(3) &= (1.-i2.) \\ (6.+i2.)X(1) + (-4.+i3.)X(2) &= (3.-i4.) \\ (5.-i) X(1) + (1.+i) X(2) + (3.+i3.)X(3) &= (5.-i6.)\end{aligned}$$

and the unknowns are X(1), X(2), and X(3).

In this case, N=3 (A is 3 by 3), and M=1. (B is 3 by 1, one right hand side).

Input:

```
INTEGER N,IA,M,IB,IJOB,IER
COMPLEX A(3,3),B(3)
REAL WA(3)
IA = 3
IB = 3
N = 3
```

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TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQT1C.

```
A =      (1.,3.)   (2.5,-3.5)   (1.,1.)
        (6.,2.)   (-4.,3.)    (0.,0.)
        (5.,-1.)   (1.,1.)     (3.,3.)

M = 1

B =      (1.,-2.)
        (3.,-4.)
        (5.,-6.)

IJOB=0
CALL LEQT1C (A,N,IA,B,M,IB,IJOB,WA,IER)
.
END

Output:

IER = 0
      (-.32881, -.68795)
B =      (-.48127, -.55729)
      (.90092, -1.5177)

Hence the solution is

X(1) = -.32881 -i0.68795
X(2) = -.48127 -i0.55729
X(3) = .90092 -il.5177
```

TABLE 4. SAMPLE EXECUTION OF THE MEAN ROTOR WAKE PROGRAM

ORIGINAL PAGE IS  
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NVANE= 11  
NBLADE= 15  
NVANE= 11  
NBLADE= 15  
HUB RADIUS DIVIDED BY DUCT RADIUS = .484  
SIGMAR= 0.4840000E+00  
VANE TIP CHORD DIVIDED BY DUCT RADIUS = .408  
SIGMAC= 0.4080000E+00  
LX0 = .6201  
LX0= 0.62010000E+00  
NDAT = ?  
NDAT= 7  
VANE GEOMETRY MATRIX INPUT  
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP  
ROW= 1 R/RDUCT = .484  
C/CTIP = 1.  
ALPHAS (DEGREES)= 16.3  
YS/CTIP = 0.  
YR/CTIP = 0.  
XS/CTIP = 0.  
XR/CTIP = 0.  
ROW= 2 R/RDUCT = .56  
C/CTIP = 1.  
ALPHAS (DEGREES)= 15.67  
YS/CTIP = .027  
YR/CTIP = -.033  
XS/CTIP = -.001  
XR/CTIP = -.02

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
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ROW= 3 R/RDUCT =  
.739  
C/CTIP =  
1.  
ALPHAS (DEGREES)=  
14.07  
YS/CTIP =  
.093  
YR/CTIP =  
-.118  
XS/CTIP =  
-.005  
XR/CTIP =  
-.057  
ROW= 4 R/RDUCT =  
.92  
C/CTIP =  
1.  
ALPHAS (DEGREES)=  
12.57  
YS/CTIP =  
.158  
YR/CTIP =  
-.213  
XS/CTIP =  
-.008  
XR/CTIP =  
-.073  
ROW= 5 R/RDUCT =  
.946  
C/CTIP =  
1.  
ALPHAS (DEGREES)=  
12.36  
YS/CTIP =  
.163  
YR/CTIP =  
-.226  
XS/CTIP =  
-.008  
XR/CTIP =  
-.07  
ROW= 6 R/RDUCT =  
.973  
C/CTIP =  
1.

TABLE 4. (Cont.)

OPTIONAL INPUT  
OF PAGE 4 OF 32

ALPHAS (DEGREES)=

12.15

YS/CTIP =

.177

YR/CTIP =

-.242

XS/CTIP =

-.009

XR/CTIP =

-.067

ROW= 7 R/RDUCT =

1.

C/CTIP =

1.

ALPHAS (DEGREES)=

11.92

YS/CTIP =

.187

YR/CTIP =

-.262

XS/CTIP =

-.009

XR/CTIP =

-.064

VANE GEOMETRY MATRIX IS

```

0.484E+00 0.100E+01 0.284E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
0.560E+00 0.100E+01 0.273E+00 0.270E-01-0.330E-01-0.100E-02-0.200E-01
0.739E+00 0.100E+01 0.246E+00 0.930E-01-0.118E+00-0.500E-02-0.570E-01
0.920E+00 0.100E+01 0.219E+00 0.158E+00-0.213E+00-0.800E-02-0.730E-01
0.946E+00 0.100E+01 0.216E+00 0.163E+00-0.226E+00-0.800E-02-0.700E-01
0.973E+00 0.100E+01 0.212E+00 0.177E+00-0.242E+00-0.900E-02-0.670E-01
0.100E+01 0.100E+01 0.208E+00 0.187E+00-0.262E+00-0.900E-02-0.640E-01

```

TYPE 1 TO INPUT ROTOR FLOW VELOCITY, 0 FOR FREE VORTEX

1

IVOR= 1

NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=

8

NVELD= 8

INPUT MATRIX FOR MEAN ROTOR FLOW

FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP

ROW= 1 R/RDUCT=

.484

MEAN CIRCUMFERENTIAL VELOCITY RATIO=

.808

ROW= 2 R/RDUCT=

.533

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

MEAN CIRCUMFERENTIAL VELOCITY RATIO= .703  
ROW= 3 R/DUCT= .612  
MEAN CIRCUMFERENTIAL VELOCITY RATIO= .734  
ROW= 4 R/DUCT= .834  
MEAN CIRCUMFERENTIAL VELOCITY RATIO= .712  
ROW= 5 R/DUCT= .918  
MEAN CIRCUMFERENTIAL VELOCITY RATIO= .688  
ROW= 6 R/DUCT= .946  
MEAN CIRCUMFERENTIAL VELOCITY RATIO= .686  
ROW= 7 R/DUCT= .974  
MEAN CIRCUMFERENTIAL VELOCITY RATIO= .713  
ROW= 8 R/DUCT= 1.  
MEAN CIRCUMFERENTIAL VELOCITY RATIO= .713  
MEAN ROTOR FLOW VELOCITY MATRIX IS  
.4840E+00 .8080E+00  
.5330E+00 .7880E+00  
.6120E+00 .7840E+00  
.8340E+00 .7120E+00  
.9180E+00 .6880E+00  
.9460E+00 .6860E+00  
.9740E+00 .7130E+00  
.1000E+01 .7130E+00  
MT = .508  
MT= 0.50800000E+00  
MA = .323  
MA = 0.32300000E+00  
WAKE WIDTH = .172  
WIDTH= 0.17200000E+00  
MAX VEL DEFICIT DIVIDED BY UBAR .27  
VELDEF= 0.27000000E+00

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

NUMBER OF RADIAL STATIONS =  
 7  
 NRAD= 7  
 NUMBER OF CHORDWISE STATIONS =  
 8  
 NCHORD= 8  
 ACCURACY OF BESSSEL FN =  
 .001  
 EB= 0.1000000E-02  
 ACCURACY OF CONVERGENCE TO ROOT XMN =  
 .0001  
 EC= 0.1000000E-03  
 S = 3  
 XMN(MAX) FOR PROPAGATION = 0.24154718E+02  
 %FRSAPR Floating underflow PC= 6115  
 %FRSAPR Floating underflow PC= 6163

## MODE DATA

S = 3 M = 1 N = 1 XMN = 0.13709056E+01  
 CUTOFF RATIO FOR MODE= .1762E+02  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.15152305E+01 BMN = -0.42119466E+00  
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 1 S = 3  
 ERROR CODE FROM INVERSION ROUTINE= 0  
 ERROR CODE FROM INVERSION ROUTINE= 0

UPSTREAM  
 GAMMA M,N,SB = 0.33725477E+02  
 MODE AMPLITUDE = 0.13613387E-03 0.33358998E-04  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7364E+02

DOWNSTREAM  
 GAMMA M,N,SB = -0.17237771E+02  
 MODE AMPLITUDE = -0.47378941E-04 -0.72085580E-05  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7715E+02

ORIGINAL PAGE IS  
OF POOR QUALITY

TABLE 4. (Cont.)

M= -1 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7364E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7715E+02

MODE DATA

S = 3 M = 1 N = 2 XMN = 0.63900327E+01

CUTOFF RATIO FOR MODE=.3780E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.19356938E+01 BMN = 0.32269858E+01

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 2 S = 3

UPSTREAM

GAMMA M,N,SB = 0.32857319E+02

MODE AMPLITUDE = -0.11049067E-03 -0.91503578E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7351E+02

DOWNSTREAM

GAMMA M,N,SB = -0.16369614E+02

MODE AMPLITUDE = 0.5e242548E-04 0.263e4856E-04

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7519E+02

M= -1 N= 2 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7351E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7519E+02

MODE DATA

S = 3 M = 1 N = 3 XMN = 0.12324612E+02

CUTOFF RATIO FOR MODE=.1960E+1

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.43514410E+01 BMN = 0.30726765E+01

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 C 0 0 0

TABLE 4. (Cont.)

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M = 1 N = 3 S = 3

## UPSTREAM

GAMMA M,N,SB = 0.30194305E+02  
MODE AMPLITUDE = -0.67274867E-04 -0.89817303E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.8036E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.13706599E+02  
MODE AMPLITUDE = 0.39056430E-04 0.46102940E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.7634E+02

M = -1 N = 3 S = -3

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.8036E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.7634E+02

## MODE DATA

S = 3 M = 1 N = 4 XMN = 0.18362274E+02  
CUTOFF RATIO FOR MODE = .1315E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.61381751E+01 BMN = 0.22116971E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 4 S = 3

## UPSTREAM

GAMMA M,N,SB = 0.24825892E+02  
MODE AMPLITUDE = 0.88119635E-06 0.55164443E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.1173E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.83381859E+01  
MODE AMPLITUDE = 0.10458061E-04 0.45172844E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.8064E+02

ORIGINAL PAGE IS  
OF POOR QUALITY

TABLE 4. (Cont.)

M= -1 N= 4 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.1173E+03

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8064E+02

LARGEST PROPAGATING N FOR THIS M = 4

MODE DATA

S = 3 M =-10 N = 1 XMN = 0.11769701E+02  
CUTOFF RATIO FOR MODE= .2052E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.54757755E+01 BMN = -0.30348594E-02  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 1 S = 3

UPSTREAM  
GAMMA M,N,SB = 0.30531741E+02  
MODE AMPLITUDE = -0.90896823E-04 0.41207877E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7690E+02

DOWNSTREAM  
GAMMA M,N,SB = -0.14044035E+02  
MODE AMPLITUDE = -0.64741460E-03 -0.25779423E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5498E+02

M= 10 N= 1 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7690E+02

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5498E+02

MODE DATA

S = 3 M =-10 N = 2 XMN = 0.16348282E+02  
CUTOFF RATIO FOR MODE= .1478E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.48044727E+01 BMN = -0.37694076E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY $M = -10 \quad N = 2 \quad S = 3$ 

## UPSTREAM

GAMMA M,N,SB = 0.27032509E+02  
MODE AMPLITUDE = 0.36213808E-04 0.13253067E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.8559E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.10544803E+02  
MODE AMPLITUDE = 0.54190425E-03 0.25744146E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5754E+02

 $M = 10 \quad N = 2 \quad S = -3$ 

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.8559E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5754E+02

## MODE DATA

S = 3    M = -10    N = 3    XMN = 0.19710760E+02  
CUTOFF RATIO FOR MODE = .1225E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.45357506E+01    BMN = -0.21469782E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

 $M = -10 \quad N = 3 \quad S = 3$ 

## UPSTREAM

GAMMA M,N,SB = 0.22996575E+02  
MODE AMPLITUDE = 0.50912282E-05 0.44796741E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.8492E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.65088688E+01  
MODE AMPLITUDE = -0.32015018E-03 -0.56725690E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5844E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= 10 N= 3 S= -3

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8492E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5844E+02

## MODE DATA

S = 3 M = -10 N = 4 XMN = 0.23588640E+02

CUTOFF RATIO FOR MODE=.1024E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.62652037E+01 BMN = -0.98372497E+00

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 4 S = 3

## UPSTREAM

GAMMA M,N,SB = 0.13736991E+02

MODE AMPLITUDE = -0.50110748E-03 -0.29130448E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6613E+02

## DOWNSTREAM

GAMMA M,N,SB = 0.27507146E+01

MODE AMPLITUDE = -0.34158767E-03 0.85520260E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6090E+02

M= 10 N= 4 S= -3

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6613E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6090E+02

LARGEST PROPAGATING N FOR THIS M = 4

## MODE DATA

S = 3 M = 12 N = 1 XMN = 0.13878611E+02

CUTOFF RATIO FOR MODE=.1740E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.60892918E+01 BMN = -0.63711792E-03

E. OR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
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M = 12 N = 1 S = 3

## UPSTREAM

GAMMA M,N,SB = 0.29133072E+02  
MODE AMPLITUDE = 0.88696711E-04 0.15987079E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.7808E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.12645367E+02  
MODE AMPLITUDE = 0.95042415E-04 0.45870526E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5892E+02

M = -12 N = 1 S = -3

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.7808E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5892E+02

## MODE DATA

S = 3 M = 12 N = 2 XMN = 0.18713666E+02  
CUTOFF RATIO FOR MODE = .1291E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.53619937E+01 BMN = -0.12842323E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 12 N = 2 S = 3

## UPSTREAM

GAMMA M,N,SB = 0.24381333E+02  
MODE AMPLITUDE = 0.31973551E-03 -0.67991251E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.6745E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.78936267E+01  
MODE AMPLITUDE = 0.14232207E-03 -0.40642054E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.6146E+02

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TABLE 4. (Cont.)

M= -12 N= 2 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6745E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6146E+02

MODE DATA

S = 3 M = 12 N = 3 XMN = 0.22297030E+02

CUTOFF RATIO FOR MODE=.1083E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.50662141E+01 BMN = -0.14574338E+01

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 12 N = 3 S = 3

UPSTREAM

GAMMA M,N,SB = 0.18059368E+02

MODE AMPLITUDE = -0.38293325E-03 -0.15805489E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6696E+02

DOWNSTREAM

GAMMA M,N,SB = -0.15716621E+01

MODE AMPLITUDE = -0.11038813E-02 0.41711175E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5569E+02

M= -12 N= 3 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6696E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5569E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

S = 3 M = -21 N = 1 XMN = 0.23254819E+02

CUTOFF RATIO FOR MODE=.1039E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.85042393E+01 BMN = -0.38116337E-05

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE IS  
OF POOR QUALITY

TABLE 4. (Cont.)

M = -21 N = 1 S = 3

UPSTREAM

GAMMA M,N,SB = 0.15145542E+02  
MODE AMPLITUDE = 0.63165623E-03 -0.10433352E-02  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5882E+02

DOWNSTREAM

GAMMA M,N,SB = 0.13421642E+01  
MODE AMPLITUDE = -0.18827030E-02 0.30355092E-02  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4796E+02

M= 21 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5882E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4796E+02

LARGEST PROPAGATING N FOR THIS M = 1  
NO MORE PROPAGATING MODES FOR THIS VALUE OF S

S = 2

XMN(MAX) FOR PROPAGATION = 0.16103146E+02

MODE DATA

S = 2 M = -3 N = 1 XMN = 0.39866274E+01  
CUTOFF RATIO FOR MODE = .4039E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.26023450E+01 BMN = -0.32589376E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 1 S = 2

ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

## UPSTREAM

GAMMA M,N,SB = 0.21981403E+02  
MODE AMPLITUDE = 0.13526694E-03 -0.11438489E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7167E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.10989599E+02  
MODE AMPLITUDE = -0.12497451E-04 -0.25469007E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6288E+02

M= 3 N= 1 S= -2

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7167E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6288E+02

## MODE DATA

S = 2 M = -3 N = 2 XMN = 0.77467003E+01  
CUTOFF RATIO FOR MODE= .2079E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.35705322E+01 BMN = -0.89511162E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 2 S = 2

## UPSTREAM

GAMMA M,N,SB = 0.20412827E+02  
MODE AMPLITUDE = -0.62938154E-04 0.18019367E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7126E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.94210234E+01  
MODE AMPLITUDE = -0.56493354E-03 0.30607513E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5566E+02

ORIGINAL PAGE IS  
OF POOR QUALITY

TABLE 4. (Cont.)

M= 3 N= 2 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7126E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5566E+02

MODE DATA

S = 2 M = -3 N = 3 XMN = 0.13008803E+02

CUTOFF RATIO FOR MODE= .1238E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = -0.18754296E+00 BMN = 0.53089865E+01

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 3 S = 2

UPSTREAM

GAMMA M,N,SB = 0.15524623E+02

MODE AMPLITUDE = -0.87384578E-05 -0.13593062E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7526E+02

DOWNSTREAM

GAMMA M,N,SB = -0.45328195E+01

MODE AMPLITUDE = 0.50005592E-03 0.24067449E-03

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5971E+02

M= 3 N= 3 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7526E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5971E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

S = 2 M = 8 N = 1 XMN = 0.96413107E+01

CUTOFF RATIO FOR MODE= .1670E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.48101923E+01 BMN = -0.14625735E-01

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY.

M = 8 N = 1 S = 2

## UPSTREAM

GAMMA M,N,SB = 0.19124322E+02  
 MODE AMPLITUDE = -0.15710355E-02 0.39986281E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4444E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.81325179E+01  
 MODE AMPLITUDE = 0.66697707E-03 -0.60581600E-04  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5598E+02

M= -8 N= 1 S= -2

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4444E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5598E+02

## MODE DATA

S = 2 M = 8 N = 2 XMN = 0.13662791E+02  
 CUTOFF RATIO FOR MODE= .1162E+01  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.41234860E+01 BMN = -0.85984376E+00  
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 8 N = 2 S = 2

## UPSTREAM

GAMMA M,N,SB = 0.14153511E+02  
 MODE AMPLITUDE = -0.50227789E-02 -0.46086629E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4172E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.31617076E+01  
 MODE AMPLITUDE = -0.18333959E-02 -0.37698765E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5006E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -8 N= 2 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4172E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5006E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

S = 2 M = -14 N = 1 XMN = 0.15975402E+02

CUTOFF RATIO FOR MODE= .1008E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.66375895E+01 BMN = -0.10554324E-03

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -14 N = 1 S = 2

UPSTREAM

GAMMA M,N,SB = 0.76348570E+01

MODE AMPLITUDE = -0.15299672E-01 0.33717128E-01

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3212E+02

DOWNSTREAM

GAMMA M,N,SB = 0.33569469E+01

MODE AMPLITUDE = 0.13580878E-01 0.28533771E-01

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3279E+02

M= 14 N= 1 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3212E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3279E+02

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS VALUE OF S

S = 1

XMN(MAX) FOR PROPAGATION = 0.80515728E+01

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

## MODE DATA

S = 1 M = 4 N = 1 XMN = 0.51995376E+01  
 CUTOFF RATIO FOR MODE= .1549E+01  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.31336383E+01 BMN = -0.20930871E+00  
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 4 N = 1 S = 1  
 ERROR CODE FROM INVERSION ROUTINE= 0  
 ERROR CODE FROM INVERSION ROUTINE= 0

UPSTREAM  
 GAMMA M,N,SB = 0.92437007E+01  
 MODE AMPLITUDE = -0.16022921E-01 -0.12244703E-01  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3113E+02

DOWNSTREAM  
 GAMMA M,N,SB = -0.37477989E+01  
 MODE AMPLITUDE = -0.10714520E-02 0.23857642E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4450E+02

M= -4 N= 1 S= -1

UPSTREAM  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.3113E+02

DOWNSTREAM  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4450E+02

LARGEST PROPAGATING N FOR THIS M = 1  
 NO MORE PROPAGATING MODES FOR THIS VALUE OF S  
 PROBLEM COMPLETED

RELATIVE POWER LEVEL UPSTREAM S= 1	-0.2812E+02
RELATIVE POWER LEVEL UPSTREAM S= 2	-0.2843E+02
RELATIVE POWER LEVEL UPSTREAM S= 3	-0.5381E+02
RELATIVE POWER LEVEL DOWNSTREAM S= 1	-0.4149E+02
RELATIVE POWER LEVEL DOWNSTREAM S= 2	-0.2964E+02
RELATIVE POWER LEVEL DOWNSTREAM S= 3	-0.4253E+02

STOP

END OF EXECUTION  
 CPU TIME: 4:39.66 ELAPSED TIME: 20:51.21  
 EXIT.

TABLE 5. INPUT/OUTPUT DATA FOR THE INLET TURBULENCE PROGRAMS

This program calculates the modal power spectral density for noise generated by a turbofan rotor subjected to inlet turbulence. All input and output data are nondimensional. The input variables are defined in order to parallel as closely as possible the variables used in the Mean Wake Program. The input data consist of geometric, performance, turbulence, and computational parameters.

## A. Geometric Data

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	NBLADE	B	No. of rotor blades	Integer
2.	SIGMAR	$\sigma_r$	Ratio of hub radius to duct radius	Floating Point
3.	SIGMAC	$\sigma_c$	Ratio of tip chord of rotor blade to duct radius	Floating Point
4.			Vector of data for a number, NDAT (an integer variable) of rotor blade radii	
a.	R	$\tilde{r}$	Nondimensional radius = $r/r_{duct}$	Floating Point
b.	C	$\tilde{c}$	Nondimensional blade chord = $c/c_{tip}$	Floating Point
c.	CHI	X	Blade angle (degrees) [See Fig. 3 of Vol. 1]	Floating Point

## B. Performance Data

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	MT	$M_t$	Tip Mach number	Floating Point
2.	MA	M	Axial flow Mach number	Floating Point
3.			Frequency range data: Pressure distributions are calculated and stored for the range of frequencies from PSTART to PEND in steps of PSTEP. These data are interpolated for calculations at the frequency of interest OMEGA.	

TABLE 5. (Cont.)

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FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
a. PSTART	-	First frequency for pressure calculation. Must be an integer multiple of shaft frequency. (Usually = NBLADE)	Integer
b. PEND	-	Final frequency for pressure calculation. See text for description of value required.	Integer
c. PSTEP	-	Frequency step size in pressure calculation. (Usually = NBLADE)	Integer
d. OMEGA	$\omega/\Omega$	Noise frequency of interest (nondimensionalized on the rotor shaft frequency)	Floating Point

## C. Turbulence Data

The inlet turbulence data are loaded into separate function subroutines. This arrangement allows rather complicated radial distributions of turbulence to be modeled.

FORTRAN FUNCTION NAME	SYMBOL	VARIABLE
1. SCALLX	$\tilde{L}_x(\tilde{r})$	Axial turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensional radius.*
2. SCALLR	$\tilde{L}_r(\tilde{r})$	Radial turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensional radius.
3. STHETA	$\tilde{L}_\theta(\tilde{r})$	Circumferential turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensional radius.*
4. EPSD	$\epsilon_D(\tilde{r})$	RMS turbulence velocity (nondimensionalized on the mean axial velocity) as a function of nondimensional radius. (See Eq. 94 of Vol. 1)

\*See page 48 of Vol. 1.

TABLE 5. (Cont.)

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## D. Computational Data

These data set the number of integration stations in the chordwise and spanwise directions (and, indirectly, the accuracy of the results). The required accuracy for the Bessel functions used in the mode shape and eigenvalue routines are also specified.

FORTRAN NAME	VARIABLE	FORTRAN VARIABLE TYPE
1. NRAD	No. of radial stations at which pressure distributions are calculated (odd number)	Integer
2. NRADNU	No. of integration stations in the chordwise direction (odd number)	Integer
3. NCHORD	No. of integration stations in the chordwise direction (even number)	Integer
4. EB	Absolute accuracy of all Bessel function calculations	Floating Point
5. EC	Absolute accuracy of convergence to annular root for boundary value problem	Floating Point

## Program Output

The output consists of the relative power spectral density for each propagating mode and for the sum of all propagating modes at the frequency of interest. The output is given in terms of the nondimensional quantity

$$10 \log_{10} \left[ \frac{S_{mn}}{\rho_0 c_0^2 r_{duct}} \right]$$

where  $S_{mn}$  is the spectral density (watt/Hz),  $\rho_0$  is the ambient air density,  $c_0$  is the small-signal speed of sound and  $r_{duct}$  is the (dimensional) duct radius. To recover the conventional spectral density (dB re  $10^{-12}$  watt/Hz) one must add

$$10 \log_{10} \left[ \frac{\rho_0 c_0^2 r_{duct}}{10^{-12} \text{ watt}} \right]$$

to the output of the program. This step is required because all computations performed in the program are nondimensional with absolute values of  $\rho_0$ ,  $c_0$ , and  $r_{duct}$  unknown.

TABLE 6. IMPORTANT INTERNAL VARIABLES FOR THE INLET TURBULENCE PROGRAM

(Used in addition to INPUT/OUTPUT Variables)

FORTRAN NAME	SYMBOL	VARIABLE
BJ(N) <sup>+</sup>	J <sub>N</sub> (X)	Nth order Bessel function of the first kind
CASCET <sup>+</sup>	Δ̄p	Stored values of the chordwise pressure distribution
H <sup>+</sup>	-	Vector length of blade spacing between corresponding points on any two neighboring blades (See Fig. B.1)
AB <sup>+</sup>	-	Nondimensional gust wave number [ $= M_t b \sigma_c (\frac{w}{\pi} - m) / M_p$ ]
LR <sup>+</sup>	L <sub>r</sub> (̄r)	Ratio of radial turbulence length scale to duct radius
LTHETA	L <sub>θ</sub> (̄r)	Ratio of circumferential turbulence length scale to duct radius
LX <sup>+</sup>	L <sub>x</sub> (̄r)	Ratio of axial turbulence length scale to duct radius
OMEGA <sup>+</sup>	ω/Ω	Ratio of noise frequency to rotor shaft frequency
OMEGBC <sup>+</sup>	-	Nondimensional acoustic wavenumber for reduced frequency [ $= M_t \sigma_c b (\frac{w}{\pi} - m)$ ]
PHIARG <sup>+</sup>	-	Argument of $\hat{\phi}_x$ (Argument)
PMNS	-	Sum of terms comprising the radial integral
QMNS	-	Sum of terms comprising the chordwise integral
RELPRL <sup>+</sup>	-	Relative modal power spectral density level at a given frequency
RELPWR <sup>+</sup> or SPWR <sup>+</sup>	-	Relative modal power spectral density at given frequency
RRRS <sup>+</sup>	R <sub>s</sub>	Weighting factor for Bessel-type integration in chordwise direction
SIGMA <sup>+</sup>	σ	Interblade phase angle (See page 52 of Vol. 1)
THEARG <sup>+</sup>	-	Argument of $\hat{\phi}_θ$ (Argument)
WHTR <sup>+</sup>	-	Weighting factor for Simpson integration in radial direction

<sup>+</sup>These variables are also used in the wake turbulence routine, but are listed here only.

TABLE 7. SAMPLE EXECUTION OF THE INLET TURBULENCE DATA  
STORAGE ROUTINE

ROTORS	ORIGINAL PART OF POOR QUALITY
NBLADE=	
15	
NBLADE= 15	
HUB RADIUS DIVIDED BY DUCT RADIUS =	
.46	
SIGMAR= 0.4600000E+00	
BLADE TIP CHORD DIVIDED BY DUCT RADIUS=	
.374	
SIGMAC= 0.3740000E+00	
NBAT =	
10	
NBAT= 10	
BLADE GEOMETRY MATRIX INPUT	
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP	
ROW= 1 R/RDUCT =	
.46	
C/CTIP =	
.628	
CHI (DEGREES)=	
3.61	
ROW= 2 R/RDUCT =	
.514	
C/CTIP =	
.662	
CHI (DEC -2S)=	
9.73	
ROW= 3 R/RDUCT =	
.541	
C/CTIP =	
.68	
CHI (DEGREES)=	
11.74	
ROW= 4 R/RDUCT =	
.622	
C/CTIP =	
.735	
CHI (DEGREES)=	
17.48	
ROW= 5 R/RDUCT =	
.73	
C/CTIP =	
.811	
CHI (DEGREES)=	
24.22	
ROW= 6 R/RDUCT =	
.838	

TABLE 7. (Cont.)

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C/CTIP =  
.887  
CHI (DEGREES)=  
30.66  
ROW= 7 R/RDUCT =  
.919  
C/CTIP =  
.945  
CHI (DEGREES)=  
35.44  
ROW= 8 R/RDUCT =  
.946  
C/CTIP =  
.959  
CHI (DEGREES)=  
37.05  
ROW= 9 R/RDUCT =  
.973  
C/CTIP =  
.976  
CHI (DEGREES)=  
38.96  
ROW= 10 R/RDUCT =  
1.  
C/CTIP =  
1.  
CHI (DEGREES)=  
41.14  
BLADE GEOMETRY MATRIX IS  
0.460E+00 0.628E+00 0.979E-01  
0.514E+00 0.662E+00 0.170E+00  
0.541E+00 0.680E+00 0.203E+00  
0.622E+00 0.735E+00 0.305E+00  
0.730E+00 0.811E+00 0.423E+00  
0.838E+00 0.887E+00 0.535E+00  
0.919E+00 0.945E+00 0.619E+00  
0.946E+00 0.959E+00 0.647E+00  
0.973E+00 0.976E+00 0.680E+00  
0.100E+01 0.100E+01 0.718E+00  
MT =  
.508  
MT= 0.50800000E+00  
MA =  
.323  
MA = 0.32300000E+00  
NUMBER OF RADIAL STATIONS =  
5  
NRAD= 5



ORIGINAL PAGE IS  
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TABLE 7. (Cont.)

NUMBER OF CHORDWISE STATIONS =  
8  
NCHORD= 8  
START FREQUENCY(HARMONIC NO. OF SHAFT )=  
15  
PSTART= 15  
END FREQUENCY(HARMONIC NO. OF SHAFT)=  
75  
P END= 75  
FREQUENCY STEP SIZE (HARMONIC ORDERS)=  
15  
PSTEP= 15  
ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)  
NASA ROTOR 53,NCHORD=8,NRAD=580Z DESIGN SPEED/9-25-9\980  
ERROR CODE FROM INVERSION ROUTINE= 0

(Note: Edited for brevity -- Error Code  
repeated for 375 inversions.)

ERROR CODE FROM INVERSION ROUTINE= 0  
STOP

END OF EXECUTION  
CPU TIME: 52:32.72      ELAPSED TIME: 1:32:28.46  
EXIT.

TABLE 8. SAMPLE EXECUTION OF THE INLET TURBULENCE NOISE  
CALCULATION

@INSRCH  
USER-ASSIGNED TITLE OF DATA SET FROM FILE "ROTO" IS  
NASA ROTOR 55,NCHORD=8,NRAD=580% DESIGN SPEED/9-25-80  
NOISE FREQUENCY/SHAFT FREQUENCY=  
15.  
OMEGA=.1500E+02  
NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=  
7  
NRADNU= 7  
ACCURACY OF BESSSEL FNS=.001  
EB=.1000E-02  
ACCURACY OF CONVERGENCE TO ROOT XMN=.0001  
EC=.1000E-03  
XMN(MAX) FOR PROPAGATION = 0.80515728E+01

*WARNING: This sample is for  
illustration purposes only.  
The input data for this  
execution did not correspond  
with Table 7 above.*

MODE DATA

OMEGA=.1500E+02 M= 0 N= 1 XMN=.0000E+00  
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.1000000E+01 BMN = 0.0000000E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 0 N= 1 OMEGA=.1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11255539E+02  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2031E-08  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8692E+02

DOWNSTREAM

GAMMA M,N,SB = -0.57596368E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=.4316E-08  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8365E+02

MODE DATA

OMEGA=.1500E+02 M= 0 N= 2 XMN=.5944E+01  
CUTOFF RATIO FOR MODE=.1354E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.17828589E+01 BMN = 0.31951480E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

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OF POOR QUALITY

TABLE 8. (Cont.)

M= 0 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.84861763E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4482E-08  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8349E+02

DOWNSTREAM

GAMMA M,N,SB = -0.29907743E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .2133E-08  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8671E+02

LARGEST PROPAGATING N FOR THIS M = 2  
ZFRSAPR Floating underflow PC= 17366

ZFRSAPR Floating underflow PC= 17433

MODE DATA

OMEGA= .1500E+02 M= 1 N= 1 XMN= .1396E+01  
CUTOFF RATIO FOR MODE=.5769E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.15347161E+01 BMN = -0.40872429E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 1 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11126733E+02  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3481E-07  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7458E+02

DOWNSTREAM

GAMMA M,N,SB = -0.56308314E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .6363E-07  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7196E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
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M= -1 N= 1 OMEGA= .1500E+02

M= -1 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.11126733E+02

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1139E-09

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9943E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.56308314E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .2030E-09

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9692E+02

## MODE DATA

OMEGA= .1500E+02 M= 1 N= 2 XMN= .6150E+01

CUTOFF RATIO FOR MODE= .1309E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.25524893E+01 BMN = 0.26060464E+01

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 1 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.82391651E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5133E-07

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7290E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.27432631E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .3747E-07

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7426E+02

M= -1 N= 2 OMEGA= .1500E+02

M= -1 N= 2 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

## UPSTREAM

GAMMA M,N,SB = 0.82391651E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3109E-09  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9507E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.27432631E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .4165E-10  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1038E+03

LARGEST PROPAGATING N FOR THIS M = 2

## MODE DATA

OMEGA= .1500E+02 M= 2 N= 1 XMN= .2748E+01  
 CUTOFF RATIO FOR MODE= .2930E+01  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.21049825E+01 BMN = -0.38973734E+00  
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 2 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.10744035E+02  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2065E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.66E5E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.52489328E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .7372E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6132E+02

M= -2 N= 1 OMEGA= .1500E+02

M= -2 N= 1 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
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## UPSTREAM

GAMMA M,N,SB = 0.10744835E+02  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.7070E-11  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1115E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.52489328E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .6529E-11  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1119E+03

## MODE DATA

OMEGA= .1500E+02 M= 2 N= 2 XMN= .6738E+01  
 CUTOFF RATIO FOR MODE= .1195E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.36099485E+01 BMN = 0.11001426E+01  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 2 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.74045386E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1927E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6715E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.19086367E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .3230E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6491E+02

M= -2 N= 2 OMEGA= .1500E+02

M= -2 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.74045386E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2280E-10  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1064E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.19086367E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .2400E-12  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1262E+05

LARGEST PROPAGATING N FOR THIS M = 2

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
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## MODE DATA

OMEGA= .1500E+02 M= 3 N= 1 XMN= .4027E+01  
 CUTOFF RATIO FOR MODE= .2000E+01  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 $\text{AMN} = 0.26815693E+01 \quad \text{BMN} = -0.27568805E+00$   
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 3 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.10115297E+02  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.8401E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6076E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.46193948E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .7621E-05  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5118E+02

M= -3 N= 1 OMEGA= .1500E+02

M= -3 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.10115297E+02  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5393E-12  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1227E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.46193948E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .6330E-13  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1320E+03

## MODE DATA

OMEGA= .1500E+02 M= 3 N= 2 XMN= .7642E+01  
 CUTOFF RATIO FOR MODE= .1054E+01  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 $\text{AMN} = 0.33544744E+01 \quad \text{BMN} = -0.11908489E+01$   
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= 3 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.54275270E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2364E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6626E+02

## DOWNSTREAM

GAMMA M,N,SB = 0.68375036E-01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .1706E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5768E+02

M= -3 N= 2 OMEGA= .1500E+02

M= -3 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.54275270E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2331E-11  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1163E+03

## DOWNSTREAM

GAMMA M,N,SB = 0.68375036E-01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .9788E-12  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1201E+03

LARGEST PROPAGATING N FOR THIS M = 2

## MODE DATA

OMEGA= .1500E+02 M= 4 N= 1 XMN= .5230E+01  
CUTOFF RATIO FOR MODE= .1539E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.32237284E+01 BMN = -0.16030403E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 4 N= 1 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
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## UPSTREAM

GAMMA M,N,SB = 0.92161443E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2038E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5691E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.37202422E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .6538E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.4185E+02

M= -4 N= 1 OMEGA= .1500E+02

M= -4 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.92161443E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5114E-13  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1329E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.37202422E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .3263E-14  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1449E+03

LARGEST PROPAGATING N FOR THIS M = 1

## MODE DATA

OMEGA= .1500E+02 M= 5 N= 1 XMN= .6376E+01  
CUTOFF RATIO FOR MODE= .1263E+01  
SUM OF BESSLE FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.37079083E+01 BMN = -0.81471940E-01  
ERROR CODE FOR BESSLE FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 5 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.79436739E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1669E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5778E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
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## DOWNSTREAM

GAMMA M,N,SB = -0.24477719E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .4521E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.3345E+02

M= -5 N= 1 OMEGA= .1500E+02

M= -5 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.79436739E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4608E-14  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1434E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.24477719E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .1763E-14  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1475E+03

LARGEST PROPAGATING N FOR THIS M = 1

## MODE DATA

OMEGA= .1500E+02 M= 6 N= 1 XMN= .7484E+01  
 CUTOFF RATIO FOR MODE= .1076E+01  
 SUM OF BESSSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.41370714E+01 BMN = -0.38730478E-01  
 ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 6 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.58865744E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4244E-04  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.4372E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.39067242E+00  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .2657E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.2576E+02

TABLE 8. (Cont.)

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M= -6 N= 1 OMEGA= .1500E+02

M= -6 N= 1 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,M,SB = 0.58865744E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3327E-15

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1548E+03

## DOWNSTREAM

GAMMA M,M,SB = -0.39067242E+00

REL. MODAL SOUND POWER SPECTRAL DENSITY= .2438E-15

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1561E+03

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS OMEGA

PROBLEM COMPLETED

RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=-.4321E+02

REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=-.2497E+02

STOP

END OF EXECUTION

CPU TIME: 3:0.55

ELAPSED TIME: 11:11.94

EXIT.

ORIGINAL COPY  
OF POOR QUALITY

TABLE 9. INPUT/OUTPUT DATA FOR THE ROTOR WAKE TURBULENCE PROGRAM

This program calculates the modal power spectral density for noise generated by the interaction of rotor wake turbulence with the stator vanes. All input and output data are nondimensional. The input variables are defined in order to parallel as closely as possible the variables used in the Mean Wake and Inlet Turbulence programs. The input data consist of geometric, performance, turbulence, and computational parameters.

A. Geometric Data

FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1. NVANE	V	No. of stator vanes	Integer
2. NBLADE	B	No. of rotor blades	Integer
3. SIGMAR	$\sigma_r$	Ratio of hub radius to duct radius	Floating Point
4. SIGMAC	$\sigma_c$	Ratio of tip chord of stator vane to duct radius	Floating Point
5.		Vector of data for a number, NDAT (an integer variable) of stator vane radii	
a. R	r	Nondimensional radius = $r/r_{duct}$	Floating Point
b. C	c	Nondimensional vane chord = $c/c_{tip}$	Floating Point
c. THETA	$\theta$	Vane angle (degrees)	Floating Point

B. Performance Data

FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1. MT	$M_t$	Tip Mach number	Floating Point
2. MA	M	Axial flow Mach number	Floating Point
3.		Frequency range data: Pressure distributions are calculated and stored for the range of frequencies from PSTART to PEND in steps of PSTEP. These data are interpolated for calculations at the frequency of interest OMEGA. See text.	

TABLE 9. (Cont.)

ORIGINAL FROM  
OF POOR QUALITY

FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
a. PSTART	-	First frequency for pressure calculation. Must be an integer multiple of shaft frequency. (Usually = NBLADE)	Integer
b. PEND	-	Final frequency for pressure calculation. (Usually = 3x NBLADE)	Integer
c. PSTEP	-	Frequency step size in pressure calculations. (Usually = NBLADE)	Integer
d. OMEGA	$\omega/\Omega$	Noise frequency of interest (non-dimensionalized on the rotor shaft frequency)	Floating Point
4. IVOR	-	Switch for rotor wake specification = 0 for free vortex distribution = 1 for specified input velocity distribution	Integer
5.	(for IVOR = 1)	Vector of data for a number, NVELO (an integer variable) of vane radii	
R	$\bar{r}$	a. Nondimensional radius	Floating Point
XVEL	$\frac{V_{yfm}}{V_{xm}}$	b. Ratio of circumferential velocity of mean wake to axial flow velocity (See Fig. 9)	Floating Point
6. MUV	$\mu_v$	(for IVOR = 0) Ratio of circumferential velocity at the duct radius to the axial flow velocity	Floating Point

## C. Turbulence Data

The wake turbulence data are assumed to be constant across the duct.

FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1. LX	$\bar{L}_x$	Axial turbulence length scale (nondimensionalized on the duct radius)	Floating Point

TABLE 9. (Cont.)

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FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
2. LR	$\bar{L}_r$	Radial turbulence length scale (nondimensionalized on the duct radius)	Floating Point
3. L'ETA	$\bar{L}_\theta$	Circumferential turbulence length scale (nondimensionalized on the duct radius)	Floating Point
4. EPSW	$\epsilon_w$	RMS turbulence velocity at wake centerline (nondimensionalized on the mean axial velocity), [see Eq. 138 of Vol. 1]	Floating Point
5. WWIDTH	$\bar{\delta}$	Ratio of turbulent wake width to duct radius (See Eq. 140 of Vol. 1)	Floating Point

## D. Computational Data

The computational input data are identical to those used for the inlet turbulence routine.

## Program Output

The output consists of the relative power spectral density for all propagating modes at the frequency of interest. The nondimensionalization used here is identical to that used for the inlet turbulence routine.

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TABLE 10. IMPORTANT INTERNAL PROGRAM VARIABLES FOR THE ROTOR  
WAKE TURBULENCE PROGRAM

(Used in addition to INPUT/OUTPUT variables)

FORTRAN NAME	SYMBOL	VARIABLE
OMEGA	$\omega/\Omega$	Ratio of noise frequency to rotor shaft frequency
FARG		Argument of $f$ (argument)
-THETA		Stator vane angle (radius)
QSUM	-	Sum of correlation function contributions multiplying pressure distribution. Value must exceed QTSTR (input variable) before pressure distribution is actually calculated.
MTHETA	-	Circumferential wake Mach number at a given radius
MYM	-	Relative circumferential wake Mach number at a given radius

TABLE 11. SAMPLE EXECUTION OF THE ROTOR WAKE TURBULENCE  
DATA STORAGE ROUTINE

ESTATOR  
NVANE= 11  
NBLADE= 15  
NBLADE= 15  
HUB RADIUS DIVIDED BY DUCT RADIUS = .484  
SIGMAR= 0.48400000E+00  
VANE TIP CHORD DIVIDED BY DUCT RADIUS= .408  
SIGMAC= 0.40800000E+00  
NDAT = 7  
NDAT= 7  
VANE GEOMETRY MATRIX INPUT  
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP  
ROW= 1 R/RDUCT = .484  
C/CTIP = 1.  
THETA (DEGREES)= 16.3  
ROW= 2 R/RDUCT = .56  
C/CTIP = 1.  
THETA (DEGREES)= 15.67  
ROW= 3 R/RDUCT = .739  
C/CTIP = 1.  
THETA (DEGREES)= 14.07  
ROW= 4 R/RDUCT = .92  
C/CTIP = 1.  
THETA (DEGREES)= 12.57  
ROW= 5 R/RDUCT = .946  
C/CTIP = 1.

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TABLE 11. (Cont.)

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THETA (DEGREES)=  
12.36  
ROW= 6 R/RDUCT =  
.973  
C/CTIP =  
1.  
THETA (DEGREES)=  
12.15  
ROW= 7 R/RDUCT =  
1.  
C/CTIP =  
1.  
THETA (DEGREES)=  
11.92  
VANE GEOMETRY MATRIX IS  
0.484E+00 0.100E+01 0.284E+00  
0.560E+00 0.100E+01 0.273E+00  
0.739E+00 0.100E+01 0.246E+00  
0.920E+00 0.100E+01 0.219E+00  
0.946E+00 0.100E+01 0.216E+00  
0.973E+00 0.100E+01 0.212E+00  
0.100E+01 0.100E+01 0.208E+00  
TYPE 1 TO INPUT ROTOR WAKE VELOCITY; 0 FOR FREE VORTEX  
1  
IVOR= 1  
NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=  
8  
NVELO= 8  
INPUT MATRIX FOR MEAN ROTOR FLOW  
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP  
ROW= 1 R/RDUCT=  
.484  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.808  
ROW= 2 R/RDUCT=  
.533  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.788  
ROW= 3 R/RDUCT=  
.612  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.784  
ROW= 4 R/RDUCT=  
.834  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.712

TABLE 11. (Cont.)

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ROW= 5 R/RDUCT= .918  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)= .688  
ROW= 6 R/RDUCT= .946  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)= .686  
ROW= 7 R/RDUCT= .974  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)= .713  
ROW= 8 R/RDUCT= 1.  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)= .713  
MEAN ROTOR FLOW VELOCITY MATRIX IS  
.4840E+00 .8080E+00  
.5330E+00 .7880E+00  
.6120E+00 .7840E+00  
.8340E+00 .7120E+00  
.9180E+00 .6880E+00  
.9460E+00 .6860E+00  
.9740E+00 .7130E+00  
.1000E+01 .7130E+00  
MT = .508  
MT= 0.50800000E+00  
MA = .323  
MA = 0.32300000E+00  
NUMBER OF RADIAL STATIONS = 5  
NRAD= 5  
NUMBER OF CHORDWISE STATIONS (.LE.20) = 8  
NCHORD= 8  
START FREQUENCY(HARMONIC NO. OF SHAFT )= 15  
PSTART= 15  
END FREQUENCY(HARMONIC NO. OF SHAFT)= 45  
PEnd= 45  
FREQUENCY STEP SIZE (HARMONIC ORDERS)= 15  
PSTEP= 15

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TABLE 11. (Cont.)

ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)  
NASA ROTOR/STATOR 55/15 BLADES,11 VANES/WAKE TURBULENCE STORAGE  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0

(Note: Edited for brevity -- Error Code  
repeated 165 times.)

ERROR CODE FROM INVERSION ROUTINE= 0  
STOP  
  
END OF EXECUTION  
CPU TIME: 21:28.07      ELAPSED TIME: 1:6:29.97  
EXIT.  
^C

TABLE 12. SAMPLE EXECUTION OF THE ROTOR WAKE TURBULENCE NOISE CALCULATION

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WASRCH  
USER-ASSIGNED TITLE OF DATA SET FROM FILE "STAT" IS  
NASA ROTOR/STATOR 55/15 BLADES,11 VANES/WAKE TURBULENCE STORAGE  
NOISE FREQUENCY/SHAFT FREQUENCY=  
15.  
OMEGA= .1500E+02  
NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=  
7  
NRADNU= 7  
ACCURACY OF BESSEL FNS= .001  
EB= .1000E-02  
ACCURACY OF CONVERGENCE TO ROOT XMN= .0001  
EC= .1000E-03  
WAKE WIDTH= .072  
WWIDTH= .7200E-01  
TURBULENCE INTENSITY(RMS FLUCTUATING U/U BAR)= .01  
EPSW= .1000E-01  
TURBULENCE LENGTH SCALE IN AXIAL DIRECTION= .5  
LX= .5000E+00  
TURBULENCE LENGTH SCALE IN RADIAL DIRECTION= .5  
LR= .5000E+00  
TURBULENCE LENGTH SCALE IN CIRCUMFERENTIAL DIRECTION= .5  
LTHETA= .5000E+00  
  
M= 0 N= 1 OMEGA= .1500E+02  
%FRSAPR Floating underflow PC= 17374  
  
%FRSAPR Floating underflow PC= 17374

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9627E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9577E+02

M= 0 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7546E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1009E+03

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TABLE 12. (Cont.)

M= 1 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8998E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1116E+03

M= -1 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1050E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9336E+02

M= 1 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8850E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9785E+02

M= -1 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1071E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9598E+02

M= 2 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8758E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9249E+02

M= -2 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1222E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9020E+02

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TABLE 12. (Cont.)

M= 2 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8410E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8596E+02

M= -2 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1090E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9225E+02

M= 3 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8632E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8503E+02

M= -3 N= 1 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1081E+03

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8705E+02

M= 3 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7849E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7829E+02

M= -3 N= 2 OMEGA= .1500E+02

UPSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9683E+02

DOWNSTREAM

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9060E+02

TABLE 12. (Cont.)

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M= 4 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8833E+02DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8132E+02

M= -4 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1006E+03DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8528E+02

M= 5 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8864E+02DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8095E+02

M= -5 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9998E+02DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8460E+02

M= 6 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8764E+02DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8147E+02

M= -6 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8544E+02DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8534E+02

PROBLEM COMPLETED

RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=-.7473E+02

REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=-.7218E+02

STOP

END OF EXECUTION

CPU TIME: 1:59.28

ELAPSED TIME: 4:6.50

EXIT.

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## PROGRAM MAINV

This is the calling program  
controlling the computation of  
mean wake/stator interaction  
noise.

PROGRAM MAINW  
DIMENSION IDATA(18),FDATA(22),VGEOU(18,7),VELOCV(12,2)  
REAL VT,VA,UV,V,LX2

C  
C  
2001 WRITE(5,2001)  
FORMAT(" NAME=")  
READ(5,1001) NAME  
1001 FORMAT(22.0)  
WRITE(5,2101) NAME  
2101 FORMAT(" NAME=",I3)  
WRITE(5,2202)  
2002 FORMAT(" VELADE=")  
READ(5,1001) VELADE  
WRITE(5,2102) VELADE  
2102 FORMAT(" VELADE=",I3)  
WRITE(5,2203)  
2003 FORMAT(" HUB RADIUS DIVIDED BY DUCT RADIUS =")  
READ(5,1001) SIGMAR  
WRITE(5,2103) SIGMAR  
2103 FORMAT(" SIGMAR=",E16.8)  
WRITE(5,2204)  
2004 FORMAT(" VANE TIP CHORD DIVIDED BY DUCT RADIUS =")  
READ(5,1001) SIGMAC  
WRITE(5,2104) SIGMAC  
2104 FORMAT(" SIGMAC=",E16.8)  
WRITE(5,2205)  
2005 FORMAT(" LX2 =")  
READ(5,1001) LX2  
WRITE(5,2105) LX2  
2105 FORMAT(" LX2=",E16.8)  
C  
C  
2006 WRITE(5,2006)  
FORMAT(" NDAT =")  
READ(5,1001) NDAT  
WRITE(5,2106) NDAT  
2106 FORMAT(" NDAT=",I3)  
WRITE(5,2207)  
2007 FORMAT(" VANE GEOMETRY MATRIX INPUT")  
WRITE(5,2108)  
2008 FORMAT(" FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP")  
C  
C  
2009 DO 10 IROW=1,NDAT  
WRITE(5,2209) IROW  
FORMAT(" P0W=",I3," R/DUCT =")  
READ(5,1001) VGEOU(IROW,1)  
WRITE(5,2110)  
2010 FORMAT(" C/CTIP =")  
READ(5,1001) VELOCV(IROW,2)  
WRITE(5,2111)

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2011 FORMAT(' ALPHAS (DEGREES)=')  
READ(5,1071) VGEOM(IROW,3)  
VGEOM(IROW,3)=VGEOM(IROW,3)\*.21\*.533  
WRITE(5,2212)  
2012 FORMAT(' VS/CTIP =')  
READ(5,1071) VGEOM(IROW,4)  
WRITE(5,2213)  
2013 FORMAT(' VF/CTIP =')  
READ(5,1071) VGEOM(IROW,5)  
WRITE(5,2214)  
2014 FORMAT(' XS/CTIP =')  
READ(5,1071) VGEOM(IROW,6)  
WRITE(5,2215)  
2015 FORMAT(' XF/CTIP =')  
READ(5,1071) VGEOM(IROW,7)  
10 CONTINUE  
C  
C  
WRITE(5,2221)  
2022 FORMAT(' VANE GEOMETRY MATRIX IS')  
DO 11 IROW=1,NROW  
WRITE(5,2127) (VGEOM(IROW,ICOLAN),ICOLAN=1,7)  
2128 FORMAT(' ',7E17.3)  
11 CONTINUE  
WRITE(5,5216)  
5222 FORMAT(' TYPE 1 TO INPUT ROTOR FLOW VELOCITY,3 FOR FREE VELOCITY')  
READ(5,1071) IVOR  
WRITE(5,5217) IVOR  
5210 FORMAT(' IVOR=',I3)  
IF (IVOR.EQ.0) NVELD=0  
IF (IVOR.EQ.0) GO TO 4005  
C  
C  
WRITE(5,3210)  
3020 FORMAT(' NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=')  
READ(5,1071) NVELO  
WRITE(5,3212) NVELO  
3032 FORMAT(' NVELO=',I3)  
WRITE(5,3214)  
3024 FORMAT(' INPUT MATRIX FOR MEAN ROTOR FLOW')  
WRITE(5,3216)  
3026 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM RUE TO TIP')  
DO 4038 IROW=1,NVELO  
WRITE(5,3218) IROW  
3008 FORMAT(' R0=',I3,' R/REDUCT=')  
READ(5,1071) VELOCV(IROW,1)  
WRITE(5,3212)  
3012 FORMAT(' MEAN CIRCUMFERENTIAL VELOCITY RATIO=')  
READ(5,1071) VELOCV(IROW,2)  
4020 CONTINUE  
C

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C

```

      WRITE(5,2114)
3014 FORMAT(" MAX FLOW VELOCITY MFTDIX IS")
      DO 1002 I30M=1,NVFLD
      WRITE(5,3116) (VELOCV(IRON,ICOLUMN),ICOLUMN=1,2)
3016 FORMAT(" ",2E16.4)
4022 CONTINUE

```

C

C

4025 CONTINUE

C

C

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```

      WRITE(5,2037)
2037 FORMAT(" MT =")
      READ(F,1071) MT
      WRITE(5,2137) MT
2137 FORMAT(" MT=",E16.6)
      WRITE(5,2031)
2031 FORMAT(" VA =")
      READ(F,1071) VA
      WRITE(5,2131) VA
2131 FORMAT(" VA =",E16.8)
      IF(TVDR.EQ.1) GO TO 6222
      WRITE(5,2032)
2032 FORMAT(" VYF/VY4 & PRODUCT =")
      READ(F,1071) VYV
      WRITE(5,2132) VYV
2132 FORMAT(" VYV =",E16.8)
      6222 CONTINUE
      IF(TVDR.EQ.1) V0V=2.
      WRITE(5,2133)
2133 FORMAT(" MAX WIDTH =")
      READ(F,1071) WIDTH
      WRITE(5,2133) WIDTH
2133 FORMAT(" WIDTH=",E16.8)
      WRITE(5,2034)
2034 FORMAT(" MAX VEL DEFICIT DIVIDED BY UPFR")
      READ(F,1071) VELDEF
      WRITE(5,2134) VELDEF
2134 FORMAT(" VELDEF =",E16.8)
C
      WRITE(5,2135)
2035 FORMAT(" NUMBER OF RADIAL STATIONS =")
      READ(F,1071) NRAD
      WRITE(5,2135) NRAD
2135 FORMAT(" NRAD=",I4)
      WRITE(5,2136)
2036 FORMAT(" NUMBER OF CHORDAL STATIONS =")
      READ(F,1071) NCORDL
      WRITE(5,2136) NCORDL

```

C <MTHEORALD>MAINV.FOR;6 Thu 3-Dec-81 1:34PM

PAGE 1:3

2136 FORMAT(" NCHORD=",I4)  
WRITE(5,2037)  
2037 FORMAT(" ACCURACY OF BESSEL FN =")  
READ(5,1001) EB  
WRITE(5,2137) EB  
2137 FORMAT(" EB=",F16.8)  
WRITE(5,2038)  
2038 FORMAT(" ACCURACY OF CONVERGENCE TO ROOT XMN =")  
READ(5,1001) EC  
WRITE(5,2138) EC  
2138 FORMAT(" EC=",F16.8)

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C  
C

IDATA(1)=NVANE  
IDATA(2)=NBLADE  
IDATA(3)=NRAD  
IDATA(4)=NCHORD  
IDATA(5)=NDAT  
IDATA(9)=IVOR  
IDATA(10)=NVELO

C  
C

RDATA(1)=MT  
RDATA(2)=MA  
RDATA(3)=LX0  
RDATA(4)=SIGMAC  
RDATA(5)=SIGMAR  
RDATA(6)=MUV  
RDATA(7)=WWIDTH  
RDATA(8)=VELDEF  
RDATA(9)=EB  
RDATA(10)=EC

C  
C

CALL SRCHV(IDATA,RDATA,VGEOM,VELOCV)  
STOP  
END

## **PROGRAM SRCHV**

Program determines which modes propagate for the mean wake/stator interaction and enables the noise calculation.

C <MTHEOBALD>SPCHV.FOR;5 Thu 3-Dec-31 1:27PM

PAGE 1

```
SUBROUTINE SPCHV(IDATA,RDATA,VGEOM,VELOCV)
INTEGER S,P1
DIMENSION IER(8),IDATA(12),M(122)
DIMENSION RDATA(28),VGEOM(12,7),POWFR(3,2),SPWR(2),RELFF(3,2)
DIMENSION VELOCV(15,2)
REAL VT,VA
```

```
C DATA((POWER(I,J),I=1,3),J=1,2)/6*3.0/
```

```
C
10 S=4
S=S-1
IF(S.LE.2) GO TO 933E
```

```
C
2007 WRITE(S,2787) S
FORMAT("S =",I2)
```

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```
C
C NNAME=IDATA(1)
NBLADE=IDATA(2)
VT=RDATA(1)
VA=RDATA(2)
STGMAX=RDATA(5)
Z=RDATA(9)
EC=RDATA(10)
```

```
C
C XMAX=S*NBLADE*VA/(1.-VA**2)**.5
```

```
C
2001 WRITE(S,2881) XMAX
FORMAT(" XMAX(VA) FOR PROPAGATION =",E16.8)
```

```
C
C P1=(S*NBLADE)/NNAME
NTEST=2*S*NBLADE-(2*P1+1)*NNAME
IF(NTEST.GT.0) P1=P1+1
```

```
C
C J=1
N(1)=S*NBLADE-P1*NNAME
```

```
C
15 N=1
20 N=N+1
```

```
C
C MBS=V(J)
IF(M(J).LT.0) MABS=-MBS
```

```
C
```

C CALL ANPT (MABS,N,SIGMAR,XMN,BMN,IER)

C C IF(XMN.GE.XMAX) GO TO 6002

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OF POOR QUALITY

C  
3002 WRITE(6,3002)  
FORMAT('2 MODE DATA')  
WRITE(6,3001) S,'(J),N,XMN  
3001 FORMAT('S =',I3,', N =',I3,', XMN =',E16.9)  
IF(YIN.EQ.0.) GO TO 1202  
COFFRA=XMAX/XMN  
WRITE(6,4001) COFFRA  
4001 FORMAT(' CUTOFF RATIO FOR MODE=',E12.4)  
GO TO 1205  
1202 CONTINUE  
WRITE(6,4002)  
4002 FORMAT(' PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')  
1205 CONTINUE  
WRITE(6,3002) IPR  
3002 FORMAT(' SUM OF BESSEL FUNCTION ERROR CODES =',I3)  
WRITE(6,3003) IEC  
3003 FORMAT(' ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

C C CALL FISGV (MABS,SIGMAR,XMN,BMN,IER)

C  
3204 WRITE(6,3204) AMN,BMN  
FORMAT(' AMN =',E16.6,' BMN =',E16.6)  
WRITE(6,3205) IPR  
3205 FORMAT(' ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC =',I1)

C C  
RDATA(11)=XMN  
RDATA(12)=AMN  
RDATA(13)=BMN  
IDATA(6)='(J)  
IDATA(7)=''  
IDATA(8)=S

C C CALL FILLOW(IDATA,RDATA,VGEOM,VFLOCY,SPWR)  
II=IABS(IDATA(3))  
POWER(II,1)=POWER(II,1)+SPWR(1)  
POWER(II,2)=POWER(II,2)+SPWR(2)

C C  
IDATA(6)=-IDATA(6)  
IDATA(8)=-IDATA(8)

C C478HFG-AID>S:CHV.FCT95 Thu 3-Dec-31 1:27PM

PAGE 102

```

C
C
      WRITE(5,8311) IDATA(6),IDATA(7),IDATA(8)
  8300    FORMAT("T= ",I5," N= ",I5," S= "I5)
      RELUP=1E.+ALOG10(SPWR(1))
      WRITE(5,8411)
  8400    FORMAT("UPSTREAM ")
      WRITE(5,8600) RELUP
  8600    FORMAT(" RELATIVE SUMD POWER LEVEL FOR MODE(M)= ",E16.4)
      RELDN=1E.+ALOG10(SPWR(2))
      WRITE(5,8200)
  8200    FORMAT("DOWNSTREAM ")
      WRITE(5,8622) RELDN
      IT=ITRS(IDATA(8))
      PWRTR(IT,1)=PWRTR(IT,1)+SPWR(1)
      PWRTR(IT,2)=PWRTR(IT,2)+SPWR(2)

```

DATA(6)=DATA(6)  
DATA(3)=DATA(8)

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OF POOR QUALITY

៦៧

6227 IF(".EQ.1) GO TO 7232

$$N \geq y = n - 1$$

REF ID: A6534

6001 FORMAT('SOLAR-GRST PROPAGATING N FOR THIS M =',I3)

IF(J.EQ.1) GO TO 5170

IF(IV(1).EQ.7) G7 TO 62P0

IF(""(J-1).LT.2) E(J+1)=E(J-1)-NVAVE

**I<sup>E</sup>(V(J-1),G^-,?)** V(J+1)=V(J-1)+NVAVE

J=J+1

GO TO 16

6100 CONTINUE  
IF("((1).LE.2) X(2)='(1)+XNAME  
IF("((1).GT.2) X(2)='(1)-XNAME  
C  
C J=2  
GO TO 15  
C  
C 6200 V(J+1)='(1)+XNAME  
J=J+1  
GO TO 15  
C  
C 7000 IF(.EQ.1) GO TO 3600  
C  
C  
C  
C 7001 WRITE(5,7011)  
FORMAT(\* NO MODE PROPAGATING MODES FOR THIS VALUE OF S\*)  
GO TO 17  
8000 CONTINUE  
WRITE(5,8011)  
FORMAT(\* NO PROPAGATING MODES FOR THIS VALUE OF S\*)  
GO TO 17  
C  
C  
9000 CONTINUE  
WRITE(5,9001)  
FORMAT(\* PROBLEM COMPLETED\*)  
DO 551 II=1,3  
DO 552 JJ=1,2  
IF(POWER(II,JJ).EQ.0.) GO TO 5215  
HELP(II,JJ)=1.\*ALOG10(POWER(II,JJ))  
GO TO 554  
5215 HELP(II,JJ)=1.E+35  
CONTINUE  
DO 637 II=1,3  
IF(ELPP(II,1).EQ.1.E+35) GO TO 5315  
WRITE(5,618) II,HELP(II,1)  
GO TO 637  
5315 WRITE(5,5618) II  
FORMAT(\* S=',I2," HARMONIC IS UNEXCITED")  
600 CONTINUE  
610 FORMAT(\* RELATIVE POWER LEVEL UPSTREAM S=\*,I2,5X,E16.4)  
DO 620 II=1,3  
IF(ELPP(II,2).EQ.1.E+35) GO TO 5415  
WRITE(5,618) II,ELPP(II,2)  
GO TO 620  
5415 WRITE(5,5618) II  
CONTINUE  
637 FORMAT(\* RELATIVE POWER LEVEL DOWNSTREAM S=\*,I2,5X,E16.4)  
RETURN  
END

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## PROGRAM FILLOV

Program computes the noise  
generated by the mean wake/  
stator interaction in a sub-  
sonic turbofan.

C <NTHFORALD>FTOLLOW.FOR,15 Thu 3-Dec-81 2:17PM PAGE 1

```
SUBROUTINE FTOLLOW(IDATA,RDATA,VGROM,VELOCV,SPWR)
DIMENSION VGROM(14,7),RDATA(27),IDATA(12),XX(6),IERPSI(2),SPWR(2)
DIMENSION PHASE(48),VELOCV(12,2)
DIMENSION PSISTD(2)
INTEGER SS,SS
REAL KX,K,YMUS,MU,MUV,NY,LY2
REAL MTHETA,MTHRUB
COMPLEX I,AF,DELTA(178),Q1NS,FVNS,TANS,ANNS
COMPLEX FVN(48)
COMPLEX Q4NST4(52,52)
COMPLEX CASCET(20,32)
DATA ISS/0/
1=(0.,1.)
FT=3.1415925
```

C  
C  
NWAVE=IDATA(1)
NPADZ=IDATA(2)
NPADY=IDATA(3)
NCNDRD=IDATA(4)
NPATE=IDATA(5)
NM=IDATA(7)
SS=IDATA(8)
IVDP=IDATA(9)
NVELD=IDATA(10)

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OF POOR QUALITY

8309  
7274  
C  
C  
NPATE(5,5377) NM,NN,SS
FORMAT('C'=',I5,' N =',I5,' S =',I5)
FORMAT(' NPAD=',I3,' NCNDR=',I3)

C  
C  
RT=RDATA(1)
R2=RDATA(2)
LYE=RDATA(3)
SIG"AC=RDATA(4)
STGMAR=RDATA(5)
NM=RDATA(6)
KVIDP=RDATA(7)
VELDZ=RDATA(8)
ZR=RDATA(9)
EC=RDATA(10)
XVN=RDATA(11)
AMN=RDATA(12)
BVN=RDATA(13)

C  
C  
SS=SS\*NPADZ

C <MTMFORMAT>FILE00.F07;15 Thu 3-5-81 2:17PM PAGE 1:1

C  
C  
7016       $BFT^S2=1.-V2**2$   
               $K^NS=((SF^"T")^2-1.57159^2*(V**2)**.5)*AS(1.^SS)/(1.^S)$   
              FOR A T (" K^NS=", E1E.4)

C  
C  
102       $WPIPA=EVF(14.733829*WPIPA**2)$   
              SIY=2.  
              SFOR=.1E-5  
              IMDX=0

102      IMDX=IMDX+1  
              DSU=1./((V5\*\*T)\*(IMDX\*\*2))  
              SVI=1. V=DSU  
              IF(DSV.LT.ERROR) GO TO 112  
              GO TO 102

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OF POOR QUALITY

C  
C  
110      XSIGY=1.  
111      GVNS=(SF^"A^NT+XSIG^"Y^"S)/FETASW  
              PVNS=(2.,%.)  
              DELTAZ=(1.-SIGMAZ)/(N=AD-1)  
              IFR=6  
              IDAT=2  
              IDOT=2

C  
C  
170      SVTP=-1.  
              DO 202 IY=1, "RAD

C  
C  
201      R=STG^AP+(1E-1.)\*(1.-SIGMAZ)/(N=AD-1.)  
              IF(P.LE.VGZOM(IDAT,1)) GO TO 221  
              IDAT=IDAT+1  
              IF(TDAT.GT.NDAT) TDAT=NDAT  
              DFLTA=(P-VGEO^((IDAT,1))/(VGEO^((TDAT,1)-VGEO^((IDAT-1,1)))  
              DO 210 IX=1,7  
210      XY((IX-1)=VGEO^((IDAT,IY)+DFLTA\*(VGEO^((IDAT,IX)-VGEO^((IDAT-1,IX)))

C  
C  
7011      Z=X^((1))/2.  
7012      ALPHAS=XX((2))  
              YS=XX((3))  
              YF=XX((4))  
              XS=XX((5))  
              XD=XX((6))  
              FORMAT(" B,ALPHAS,YS,YF,XS,XD OF R IS")  
              FORMAT(6E1E.4)

C  
C  
102      IF(TVOR.EQ.7) GO TO 412

C-2

C <MTHEOFALD>FILED, FEB 15 THU 3-DEC-81 2:17 PM PAGE 12

C  
C  
C INTERPOLATE TO GET MEAN CIRCUMFERENTIAL MACH NUMBERS AT THIS A

```

4881 IF(F.LE.VELLOCV(IDOT,1)) GO TO 4881
      IDOT=IDOT+1
      IF(IDOT.GT."VEL") IDOT="VEL"
      DELTA=(R-VELLOCV(IDOT,1))/(VELLOCV(IDOT,1)-VELLOCV(IDOT-1,1))
      XVEL=VELLOCV(IDOT,2)+DELTA*(VELLOCV(IDOT,2)-VELLOCV(IDOT-1,2))
      XTHI=VELLOCV(IDOT,3)

```

C 4615 FORMAT(“E=”,E11.4,“VIBRATIONS”,E11.4)

4020      I<sup>E</sup>(IR.EQ.1) V<sup>THUB=VTHETA</sup>  
CONTINUE

**ORIGINAL PAGE IS  
OF POOR QUALITY**

WV=AT,T=H-MAV+UV/R  
IF(IVDR.EQ.1) IV=IVT+R-MVHETP  
ACL=ATAVZ(NVH,13)

$$\begin{aligned}\cos A &= \cos(\alpha + \beta) \\ \sin A &= \sin(\alpha + \beta)\end{aligned}$$

```

P1=RT1=LXZ*(V1/SIGMAR*2-1./R**2)
IF(TVOR.EQ.1) P1=RT1=LXZ*(V1/SIGMAR*2-ATHTET1/V1/R)
P1=RT2=STG*AC*(Y5+Y7)/2
P1=RT3=STG*AC*(X5+X7)*(V1/V1-VUVV/R**2)
IF(TVOR.EQ.1) P1=RT3=STG*AC*(X5+X7)*(VT/V1-ATHTET1/V1/R)

```

4715E1 = E2-(FACT1-PART1-FAPT1)

PHASE2=SIN(STG\*180PI/(SINAS+COSAS\*NY/144))/R

$\text{W} = (\text{VELD} * \text{F} / \text{SW}) * \sin(\text{ICL} + \text{ALP} + \text{S}) * \text{WETA} * (-\text{SS} * \text{x2})$   
 $\text{WH} = \text{V} * \text{CEYD}(-\text{I} * (\text{PHASE1} + \text{PHASE2}))$

KY=-PHASE2

```

MFB=44*(1.+(TUVF/R)**2)**0.5
IF(TVDF.EQ.0.1) MFB=(MFB**2+ATRDT4**2)**0.5

```

C <4THFOTALD>FTLLOV.FD-215 Thu 3-Dec-61 3:17 PM PAGE 103

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OF POOR QUALITY**

$$K = S^2 \times V_2 \times S^2 \times STG \times S^2 / (1, -1, z^{1/2})$$

$$GA^{V\rightarrow I} = (2.053 \cdot PI / VVA^S) \cdot (1. + V T^P \cdot V R^P K^P S I N K^P S / (1. - V R^P \cdot Z))$$

$$H_1 = -2 \cdot p_T \cdot \sin(\theta) / (\sqrt{s} \cdot \cos(\phi))$$

$$H_2 = 2 \cdot p_T \cdot \cos(\theta) / (\sqrt{s} \cdot \sin(\phi))$$

~~SKIP CALL AND STOP OF PAGES FOR DOWNSTREAM  
IF(YSTGK.EQ.-1.) GO TO 332~~

SKIP PRES CALL AFTER READ CALLS FOR THIS VALUE OF S(=SS)  
I'(SS.EQ.ISS) GO TO 328

## 307 FORMAT('INPUT TO SUBROUTINE PRES')

302 ԵՐԵՎԱՆ ( ՀԻԿ- 1216.4 )

384 :GxVAT("xy=",E16.4,"y=",E16.4,"GxVAT=",E16.4)

246 291ITE(21,325) 43,51,E2,VCHECR  
COLMATE 10-1982 2 1982

```
FORMAT( '%%=.,%15.4,,%%=1E.4,,%%E15.4,,%%CRD=,,%33
```

CALL PREF((1,1,1),X,Y,Z,SAVMA,45,81,82,NCHECKD,DELTAB,LEB2)

IF(75.32.48.10) ISS=SS

DE 310 100-1, MCHORD

**CASET(ICK, ICK) = DELTA(ICK)**

三

אלה נזק (הנזהר, גזע)

7625  $\text{P} = \text{P} + (\text{P} - \text{P}_{\text{REF}}) \cdot (\text{DELTA P}(\text{I}2), \text{IG}=1, \text{NCHCF})$   
 $(\text{D} = \text{LTP}(\text{I}4), \text{I}2=1, \text{NCHDRD})$

~~CONTINUE  
ZEND=SIGNAL(R\*(G4\*S\*CDSAS-KV-SINAS/?)~~

Q"AS=CASCET(IP,NCHOFD)/3.  
Q"NST"(TR,NCHOFD)=Q"AS  
S"TC=1.

SEARCHED **<NTHEOPALD>PTLLOV**. FILED 2:15 PM THU 3-DEC-81 2:17 PM PAGE 1:4

```

270      CONTINUE
A'V,S=-PVNS*WAVE*SIGMAC/(PI*(1.-SIGMA**2))
C
FOR "UM=2,*K" I=1,N,1 CABS(PVNS)*PVNS+WAVE*SIGMAC)**2
PVNS=PI*(1.-SIGMA**2)*((SE*AT)+XSIGV*MA*VMNS)**2
RELPOWER=PVNS/4/PD*DE
RELPOWER=10.*LOG10(RELPOWER)
C
CC
C
I=(XSIGV.LT.0.) G7 TO 9201
C
C
WRITE(5,3200)
3000 FORMAT("UPSTREAM")
WRITE(5,8101) G'NS
8101 FOR"LT(" GAMMA N,N,SE =",E16.8)
WRITE(5,5122) AMNS
8102 FOR"LT(" MODE AMPLITUDE =",E16.8)
WRITE(5,8522) IER
8500 FORMAT(" SUM OF ALL ERRORS IN PSI CALCULATIONS =",I5)
WRITE(5,8602) RELPRL
8600 FORMAT(" RELATIVE SOUND POWER LEVEL FOR MODE(0)=",E16.4)
DO 7000 IR=1,HEAD
      P=SIGMAR+(IR-1.)*(1.-SIGMAR)/(VRAD-1.)
7002 FOR"AT(5X,E17.4)
7006 CONTINUE
7200 FORMAT(" END OF UPSTREAM INTEGRATION")
YSIGV=1.
SPVP(1)=RELPVR
      G7 TO 111
9000 WRITE(5,8200)
8200 FORMAT("DOWNSTREAM")
WRITE(5,8201) G'NS
8201 FOR"AT(" GAMMA N,N,SE =",E16.8)
WRITE(5,8202) AMNS
8202 FOR"AT(" MODE AMPLITUDE =",E16.8)
WRITE(5,8402) IER
8400 FORMAT(" SUM OF ALL ERRORS IN PSI CALCULATIONS =",I5)
WRITE(5,8502) RELPRL
SPVP(2)=RELPVR
7202 FORMAT(" END OF DOWNSTREAM INTEGRATION")
RETURN
END

```

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## **PROGRAM MAINTI**

**This is a calling program to  
control the computation of  
pressure data for the inlet  
turbulence case.**

```
PROGRAM MAINTI
DIMENSION IDATA(10),RDATA(20),VGEOM(10,7)
REAL MI,MA
INTEGER PSTART,PEND,P,PRANGE,PSTEP
DATA (IDATA(J),J=1,10)/10*0/
DATA (RDATA(J),J=1,20)/20*.0.0/
```

C  
C ROTOR INFLOW TURBULENCE -- MATRIX STORAGE PROGRAM

C THIS PROGRAM GROUP CALCULATES AND STORES VECTORS OF
C THE COMPLEX PRESSURE DISTRIBUTION ACROSS THE ROTOR BLADE.

C DATA REQUIRED TO EXECUTE THIS ROUTINE INCLUDE:

- C 1. BLADE GEOMETRY
- C 2. ROTOR OPERATING SPEEDS
- C 3. NUMBER OF RADIAL AND CHORDWISE POSITIONS AT WHICH THE
 C PRESSURES ARE CALCULATED
- C 4. FREQUENCY RANGE OF INTEREST (EXPRESSED IN TERMS
 C OF HARMONIC ORDER OF SHAFT ROTATION).

C THE RANGE OF CIRCUMFERENTIAL MODE NUMBER M IS 0 TO NBLADE-1.

C NCHORD MUST BE NO GREATER THAN 20.

```
1891 FORMAT(G20.8)
      WRITE(5,2002)
2002 FORMAT(" NBLADE=")
      READ(5,1001) NBLADE
      WRITE(5,2102) NBLADE
1002 FORMAT(" NBLADE=",I3)
      WRITE(5,2003)
2003 FORMAT(" HUB RADIUS DIVIDED BY DUCT RADIUS =")
      READ(5,1001) SIGMAR
      WRITE(5,2103) SIGMAR
2103 FORMAT(" SIGMAR=",E16.8)
      WRITE(5,2004)
2004 FORMAT(" BLADE TIP CHORD DIVIDED BY DUCT RADIUS=")
      READ(5,1001) SIGMAC
      WRITE(5,2104) SIGMAC
2104 FORMAT(" SIGMAC=",E16.8)
C
C
2006 FORMAT(" NDAT =")
      READ(5,1001) NDAT
      WRITE(5,2106) NDAT
2106 FORMAT(" NDAT=",I3)
      WRITE(5,2007)
```

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```
2887 FORMAT(" BLADE GEOMETRY MATRIX INPUT")
      WRITE(5,2008)
2888 FORMAT(" FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP")
C
C
2889 DO 10 IROW=1,NDAT
      WRITE(5,2009) IROW
      FORMAT(" ROW=",I3," R/RDUCT =")
      READ(5,1001) VGEOM(IROW,1)
      WRITE(5,2010)
      FORMAT(" C/CTIP =")
      READ(5,1001) VGEOM(IROW,2)
      WRITE(5,2011)
      FORMAT(" CHI (DEGREES)=")
      READ(5,1001) VGEOM(IROW,3)
      VGEOM(IROW,3)=VGEOM(IROW,3)*.0174533
      CONTINUE
C
C
2828 WRITE(5,2020)
      FORMAT(" BLADE GEOMETRY MATRIX IS")
      DO 11 IROW=1,NDAT
      WRITE(5,2120) (VGEOM(IROW,ICOLMN),ICOLMN=1,3)
      FORMAT(" ",7E16.3)
      11 CONTINUE
C
C
2830 WRITE(5,2030)
      FORMAT(" MT =")
      READ(5,1001) MT
      WRITE(5,2130) MT
2130 FORMAT(" MT=",E16.8)
      WRITE(5,2031)
      FORMAT(" MA =")
      READ(5,1001) MA
      WRITE(5,2131) MA
      2131 FORMAT(" MA =",E16.8)
C
C
2835 WRITE(5,2035)
      FORMAT(" NUMBER OF RADIAL STATIONS =")
      READ(5,1001) NRAD
      WRITE(5,2135) NRAD
2135 FORMAT(" NRAD=",I4)
      WRITE(5,2036)
      FORMAT(" NUMBER OF CHORDWISE STATIONS =")
      READ(5,1001) NCHORD
      WRITE(5,2136) NCHORD
2136 FORMAT(" NCHORD=",I4)
```

C <MTHEUBALU>MAINTI.FOR;13 wed 24-Sep-88 3:23PM PAGE 1:2

C  
C        WRITE(5,100)  
100      FORMAT(" START FREQUENCY(HARMONIC NO. OF SHAFT) =")  
        READ(5,1001) PSTART  
        WRITE(5,110) PSTART  
110      FORMAT(" PSTART = ",I4)  
        WRITE(5,120)  
120      FORMAT(" END FREQUENCY(HARMONIC NO. OF SHAFT) =")  
        READ(5,1001) PEND  
        WRITE(5,130) PEND  
130      FORMAT(" PEND = ",I4)

C  
C

          WRITE(5,140)  
140      FORMAT(" FREQUENCY STEP SIZE (HARMONIC ORDERS) = ")  
        READ(5,1001) PSTEP  
        WRITE(5,150) PSTEP  
150      FORMAT(" PSTEP = ",I4)  
        PRANGE=(PEND-PSTART)/PSTEP+1  
        IDATA(2)=NBLADE  
        IDATA(3)=NRAD  
        IDATA(4)=NCHORD  
        IDATA(5)=NDAT  
        IDATA(6)=PSTART  
        IDATA(7)=PEND  
        IDATA(8)=PSTEP

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C  
C

RDATA(1)=MT  
RDATA(2)=MA  
RDATA(4)=SIGMAC  
RDATA(5)=SIGNAR

C  
C

CALL ROTOKS(IDATA,RDATA,VGEOM)  
STOP  
END

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## PROGRAM ROTORS

Program calculates and stores  
the pressures generated on a  
turbofan rotor by inlet tur-  
bulence.

C C11000HLLPJKUJURD.FUR;14 WED 23-SEP-81 9:31AM PAGE 1

SUBROUTINE ROTURS(IUATA,RDATA,VGUM)

ADJUSTABLE DIMENSION STATEMENTS USED TO MINIMIZE STORAGE  
REQUIREMENTS OF MATRIX CASCET

DIMENSION OF DELTAP=20

DIMENSION OF CASCET=(NCHORD,NRAU,NBLACE,PRANGE)

MATRIX NUMBER MUST BE NO GREATER THAN 20

DIMENSION DELTAP(20)

DIMENSION VGUM(12,7),RUATA(23),IUATA(12),XX(6)

DIMENSION CASCET(5,5,10,5)

DIMENSION A(72)

REAL KA,MP,MA,MT

COMPLEX I,DELTAP,CASCET

INTEGER PSTART,PEND,P,PRANGE,PSTEP

I=(0,1,)

P1=3.1415920

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OF POOR QUALITY

NBLACE=IUATA(2)

NRAU=IUATA(3)

NCURKU=IUATA(4)

NUAL=IUATA(5)

PSTART=IUATA(6)

PEND=IUATA(7)

PSTEP=IUATA(8)

RI=RUATA(1)

RA=RUATA(2)

SIGMAC=RUATA(4)

SIGMAR=RUATA(5)

INITIALIZE IUAT FOR GEOMETRIC DATA

IUAT=2

WRITE(5,100)

100 FORMAT("ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)")  
READ(5,100),A

1003 FORMAT(72A1)

START LUMPED IN CABLE CROSS-SECTION WITH LUMP ON RADIAL  
POSITION TO MINIMIZE INTERPOLATION.

DO 390 IX=1,NRAU

R=SIGMAP+(IR-1)\*(1.-SIGMAR)/(NRAU-1.)  
 IF(R.LE.VGEUM(IUAT,1)) GO TO 201  
 IUAT=IUAT+1  
 IF(IUAT.GT.NUAT) IUAT=NUAT  
 201 DELTA=(M-VGEUM(IUAT,1))/(VGEUM(IUAT,1)-VGEUM(IUAT-1,1))  
 DO 213 IA=2,3  
 213 AL(IA-1)=VGEUM(IUAT,IX)+DELTA\*(VGEUM(IUAT,IX)-VGEUM(IUAT-1,IA))

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OF POOR QUALITY

201

213

C

C

B=AA(1)/2.  
 AA1=AA(2)  
 WRITE(21,7010) B,CHI,R

7010

FORMAT(" B=",E10.4," CHI=",E10.4," R=",E10.4)

C

C

C

CUSCHI=CUS(CHI)  
 SINCHI=SIN(CHI)

C

C

C

BEGIN LOOPS ON MODE NUMBER M AND FREQUENCY COUNTER P

DO 300 MOUNT=1,NOMOD  
 MM=MOUNT-1

C

C

C

IP IS STORAGE COUNTER FOR PARAMETER P IN MATRIX CASCET  
 IP=?

C

C

C

DO 310 P=PSTART,PEND,PSTEP  
 IP=IP+1

C

C

C

MH=MH\*2+SIUMAC\*D\*(P-MM)

C

C

C

MH=(MH\*2+(MT\*D)\*2)\*T.5

C

C

C

MD=M2/MR\*D\*SIUMAC\*(P-MM)  
 SIUMAC=-2.\*PI\*M/NBLAUS

C

C

C

D=2.\*PI\*R/MOUNT/SIUMAC/D

C

```

381      WRITE(21,300)
382      FORMAT("INPUT TO SUBROUTINE CASC")
383      WRITE(21,302) OMEGAC
384      FORMAT(" OMEGAC=",L12.4)
385      WRITE(21,314) MR,KB,SIGMA
386      FORMAT(" MR=",E18.4," KB=",E18.4," SIGMA=",E18.4)
387      WRITE(21,310) n,Cn1,NCHORD
388      FORMAT(" n=",E18.4," Cn1=",E18.4," NCHORD=",I3)

```

C

C

C

C

CALL CASC(OMEGAC,MR,KB,SIGMA,n,Cn1,NCHORD,DELTAP,IERP)

STORE RESULTS OF CASC IN STOREAGE MATRIX FOR VDISK FILE.  
MATRIX POSITION DESCRIPTORS ARE (IN ORDER OF APPEARANCE):

1. CHOROIDAL POSITION (TRAILING TO LEAVING EDGES)
  2. RADIAL POSITION (INNER RADIUS TO OUTER RADIUS)
  3. CIRCUMFERENTIAL MODE NUMBER + 1 ( $m+1$ )
  4. ORDER OF FREQUENCY COMPUTATIONS (FIRST TO LAST)
- WITH: IP=1 FOR PSTART  
IP=PRANGE FOR PEND

C

C

C

```

      DO 310 13=1,NCHORD
      CASCET(13,1K,NCJUNCT,1P)=DELTAP(13)
310      CONTINUE
      WRITE(5,7503) IERP
7503      FORMAT(" ERROR CODE FROM INVERSION ROUTINE=",I3)
      WRITE(21,7025)
7025      FORMAT(" OUTPUT FROM CASC:(DELTAP(14),14=1,NCHORD")
      WRITE(21,7032) (DELTAP(14),14=1,NCHORD)
5004      FORMAT(5A,OE18.4)

```

C

C

C

320 CONTINUE

C

STORE MATRIX OF PRESSURE VALUES ON THE VDISK FOR LATER  
PROCESSING BY OTHER PROGRAMS.

C

CALL OFILE(23,"ROTO")  
 WRITE(23) A  
 WRITE(23) IDATA  
 WRITE(23) RDATA  
 WRITE(23) V620M  
 WRITE(23) CASCET

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C <MTHEUDALDPRUTORS.FOR> 14 wed 23-sep-01 9:31AM PAGE 1:3

C  
C  
C  
ENDFILE 23

STOP  
END

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## **PROGRAM INSRCH**

**Program determines which modes  
propagate for the case of inlet  
turbulence and controls the  
noise computation.**

```
PROGRAM INSRCH
DIMENSION CASCET(8,5,15,5)
DIMENSION IER(8),IDATA(18)
DIMENSION RDATA(20),VGEOM(10,7),POWER(2),SPWR(2),RELPR(2)
DIMENSION NPCON(4)
DIMENSION A(72)
INTEGER PRANGE,PEND,PSTART,PSTEP
COMPLEX CASCET
REAL MT,MA
```

```
      DATA(POWER(J),J=1,2)/2*0.8/
```

```
C
C
C
C CALLING PROGRAM FOR INTUR3 TO SEARCH OUT AND CALCULATE
C ALL PROPAGATING MODES AT A GIVEN POSITIVE FREQUENCY.
```

```
C
C
C
C OPEN FILE "ROTO" AND READ INPUT ARRAYS
C INCLUDING MAIN STORAGE MATRIX "CASCET".
```

```
C*****NOTE THAT "ROTO" IS A SEQUENTIAL UNFORMATTED BINARY FILE--
C
C ORDER OF STORAGE=A, IDATA, RDATA, VGEOM, CASCET
C*****
```

```
CALL IFILE(23,"ROTO")
READ (23) A
READ (23) IDATA
READ (23) RDATA
READ (23) VGEOM
READ (23) CASCET
ENDFILE 23
```

```
5      WRITE(5,5)
      FORMAT(" USER-ASSIGNED TITLE OF DATA SET FROM FILE "ROTO" IS")
      WRITE(5,6) A
      FORMAT(" ",72A1)
      PSTART=IDATA(5)
      PEND=IDATA(7)
      PSTEP=IDATA(8)
      PRANGE=(PEND-PSTART)/PSTEP+1
      NPCON(1)=PSTART
      NPCON(2)=PEND
      NPCON(3)=PSTEP
      NPCON(4)=PRANGE
```

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**C**      ENTER NOISE FREQUENCY OF INTEREST(MUST BE POSITIVE FREQUENCY)

```
1001 FORMAT(G20.8)
      WRITE(5,119)
119  FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')
      READ(5,1001) OMEGA
      RDATA(8)=OMEGA
115  FORMAT(' OMEGA=',E10.4)
      WRITE(5,115) RDATA(9)
```

C SELECT NO. OF RADIAL POSITIONS TO INTERPOLATE PRESSURES  
C (ASSUMED THAT NRADNU.GE.NRAD)

**C\*\*\*\*\*NOTE: NRADNU MUST BE .LE.30 UNLESS DIMENSION STATEMENTS IN  
C "INTURB" ARE TO BE MODIFIED**

```

120  WRITE(5,120)
      FORMAT(" NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=")
      READ(5,1001) NRADNU
      IDATA(1)=NRADNU
      WRITE(5,130) IDATA(1)
      FORMAT(" NRADNU=",I4)
      WRITE(5,2037)
2037  FORMAT(" ACCURACY OF BESSEL FNS=")
      READ(5,1001) EB
      WRITE(5,2137) EB
2137  FORMAT(" EB=",E10.4)
      WRITE(5,2038)
2038  FORMAT(" ACCURACY OF CONVERGENCE TO ROOT XMN=")
      READ(5,1001) EC
      WRITE(5,2138) EC
2138  FORMAT(" EC=",E10.4)
      RDATA(9)=EB
      RDATA(10)=EC
      MT=RDATA(1)
      MA=RDATA(2)
      SIG4AR=RDATA(5)

```

$$X_{MAX} = \text{OMEGA}^* \text{QT} / (1. - \text{MA}^{**2})^{**.5}$$

WRITE(5,2001) XMAX  
2001 FORMAT(" XMN(MAX) FOR PROPAGATION =",516.8)

C START WITH PLANE WAVE MODE (0,1). COUNT UP IN N, THEN M  
C UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

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J=1  
N=0

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RESTART N COUNT HERE FOR NEW N

N=0

INCREMENT N

N=N+1

MABS=IABS(M)

CALL ABRT (MABS,N,SIGNAR,E8,EC,XMN,IE8,IEC)

IF MODE IS CUT OFF, GO TO 6000

IF(XMN.GE.XMAX) GO TO 6000

WRITE(5,3000)

FORMAT("64ODE DATA")

WRITE(5,3001) OMEGA,M,N,XMN

3001 FORMAT("OMEGA=",E10.4," M=",I3," N=",I3," XMN=",E10.4)

IF(XMN.EQ.9.) GO TO 1000

COPFRA=XMAX/XMN

WRITE(5,4000) COPFRA

4000 FORMAT(" CUTOFF RATIO FOR MODE=",E10.4)

GO TO 1005

1000 CONTINUE

WRITE(5,4005)

4005 FORMAT(" PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE")

1005 CONTINUE

WRITE(5,3002) IEB

3002 FORMAT(" SUM OF BESSE: FUNCTION ERROR CJ0ES =",I3)

WRITE(5,3003) IEC

3003 FORMAT(" ERROR CODE FOR CONVERGENCE TO ROOT XNN =",I3)

NORMALIZE MODE AMPLITUDE

CALL EIGEN (MABS,SIGNAR,XMN,AMN,BMN,E8,IER)

WRITE(5,3004) AMN,BMN

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3004 FORMAT(" AMN =",E16.8," BMN =",E16.8)  
3005 WRITE(5,3005) IER  
FORMAT(" ERROR CODE FOR BESSEL FUN IN AMN AND BMN CALC =",8I2)

C  
C

RDATA(11)=XMN  
RDATA(12)=AMN  
RDATA(13)=BMN  
IDATA(6)=M  
IDATA(7)=N

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C  
C

CALL INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)  
POWER(1)=POWER(1)+SPWR(1)  
POWER(2)=POWER(2)+SPWR(2)

C  
C  
C

DO NOT SWITCH SIGN ON M IF M=0

C IF(M.EQ.0) GO TO 20

C IDATA(6)=-IDATA(6)

C  
C

8309 WRITE(5,8309) IDATA(6),IDATA(7),RDATA(8)  
FORMAT("0M=",I5," N=",I5," OMEGA=",E16.4)

C SWITCH SIGN ON M AND RECALCULATE

C

CALL INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)  
POWER(1)=POWER(1)+SPWR(1)  
POWER(2)=POWER(2)+SPWR(2)

C  
C

IDATA(6)=-IDATA(6)

C GO TO 20

C  
C  
C  
C

C IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.

C 6500 IF(N.EQ.1) GO TO 7000

C

NMAX=N-1  
WRITE(5,6501) NMAX

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6001 FORMAT("LARGEST PROPAGATING N FOR THIS M =",I3)

C

C

J=J+1

C

C

INCREMENT M

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OF POOR QUALITY

C

M=M+1  
GO TO 15

C

C

C

N=1 TO REACH THIS POINT

7000 CONTINUE

C

C

WRITE(5,7001)

7001 FORMAT(" NO MORE PROPAGATING MODES FOR THIS OMEGA")

10

CONTINUE

WRITE(5,9001)

9001 FORMAT(" PROBLEM COMPLETED")

DO 550 JJ=1,2

IF(POWER(JJ).EQ.0.) GO TO 5215

RELPR(JJ)=10.\* ALOG10(ABS(POWER(JJ)))

GO TO 550

5215

RELPR(JJ)=1.E+35

550

CONTINUE

IF(RELPR(1).EQ.1.E+35) GO TO 5315

WRITE(5,610) RELPR(1)

GO TO 600

5315

WRITE(5,5510)

5610

FORMAT(" FREQUENCY IS CUT OFF")

600

CONTINUE

610

FORMAT(" RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=",E10.4)

IF(RELPR(2).EQ.1.E+35) GO TO 5415

WRITE(5,630) RELPR(2)

GO TO 620

5415

WRITE(5,5610)

620

CONTINUE

630

FORMAT(" REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=",E10.4)

STOP

END

## **PROGRAM INTURB**

**Program computes the noise  
generated by a turbofan rotor  
subjected to inlet turbulence.**

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SUBROUTINE INTURB(IDATA,RDATA,VGEOM,SPWR,CASSET,NPCON)

PROGRAM COMPUTES THE SOUND POWER GENERATED BY A TURBOFAN ROTOR SUBJECTED TO INLET TURBULENCE. THIS IS A SIMPLIFIED VERSION SUITABLE FOR VERY SMALL TURBULENCE LENGTH SCALES IN THE RADIAL DIRECTION

PROGRAM INTERPOLATES IN RADIAL POSITION AND FREQUENCY FROM A STORED MATRIX OF PRESSURE DISTRIBUTIONS (NAME=CASSET)

```
DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6),IERPSI(2),SPWR(2)
DIMENSION BJ(20)
DIMENSION CASSET(8,5,15,5)
DIMENSION PSISTO(30),NPCON(4),RR(30),RRNU(30)
INTEGER P,PSTEP,PRANGE,PSTART,PEND
REAL KMNS,MT,VA,LR,LTHETA,LX
COMPLEX I,DELTAP,QMNS,CASSET
COMPLEX Z,RRS,RRRS,QMNST
COMPLEX Y
```

C \*\*\*\*\*  
C DIMENSION OF PSISTO AND RRNU MUST BE .GE. NRADNU  
C DIMENSION OF RR MUST BE .GE. NRAD

I=(0.,1.)  
PI=3.1415926

```
NRADNU=IDATA(1)
NBLADE=IDATA(2)
NRAD=IDATA(3)
NCHORD=IDATA(4)
NDAT=IDATA(5)
MM=IDATA(6)
NN=IDATA(7)
OMEGA=RDATA(8)
PRANGE=NPCON(4)
PSTART=NPCON(1)
PEND=NPCON(2)
PSTEP=NPCON(3)
SIGMAR=RDATA(9)
```

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```
8300 WRITE(5,8300) MM,NN,OMEGA
      FORMAT("MM=",15,"   NN=",15,"   OMEGA=",E18.4)
      WRITE(21,8300) MM,NN,OMEGA
      WRITE(21,700)
```

C <MTHEUHALU> INTURB.FOR,40 Mon 29-Sep-80 10:13AM PAGE 1:1

```
198      FORMAT(" INTURB EXECUTION")
          WRITE(21,7204) NRAD,NCHORD
7204      FORMAT(" NRAD=",I3," NCHORD=",I3)
```

C LIST NONDIMENSIONAL RADIAL POSITIONS AVAILABLE IN STORED  
C DATA (NEEDED FOR INTERPOLATION)

```
DO 5 IR=1,NRAD
R=SIGMAR+(IR-1.)*(1.-SIGMAR)/(NRAD-1.)
RR(IR)=R
CONTINUE
```

5

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```
WRITE(21,6)
FORMAT(' R VALUES FROM STURAGE ARE')
WRITE(21,8) RR
FORMAT(7E10.4)
```

```
MT=RDATA(1)
MA=RDATA(2)
SIGMAC=RDATA(4)
EB=RDATA(9)
EC=RDATA(10)
XMN=RDATA(11)
AMN=RDATA(12)
BMN=RDATA(13)
```

INITIALIZE ERROR ACCUMULATOR IN PSI CALCULATIONS  
1E-8

**LIST NONDIMENSIONAL RADIAL POSITIONS TO BE USED IN INTERPOLATION**

```

DO 7 IRNU=1,NRADNU
K=SIGMAR*(IRNU-1.)*(1.-SIGMAR)/(NRADNU-1.)
RRNU(IRNU)=R

```

**COMPUTE AND STORE MODE SHAPE WEIGHTING AT EACH RADIUS**

```

      ARG<MM*R-
      CXL-RMODE(MM,ARG,AMN,BMN,PSI,EB,IERPSI)
      PSI=STO(IRNU)=PSI
      IEN=IER+IERPSI(1)+IERPSI(2)

```

**CONTINUE**

C  
C  
9        WRITE(21,9)  
      FORMAT(" R VALUES FOR INTERPOLATION ARE")  
      WRITE(21,8) RRNU  
11        WRITE(21,11)  
      FORMAT(" PSIST0 VALUES ARE")  
      WRITE(21,3) PSIST  
  
C  
C  
12        BETASQ=1.-MA\*\*2  
      KMNS=((OMEGA\*MT)\*\*2-BETASQ\*XMN\*\*2)\*\*.5)\*ABS(OMEGA)/OMEGA  
      WRITE(21,7C18) KMNS  
7018        FORMAT(" KMNS=",310.4)  
  
C  
C  
13        CHECK TO BE SURE MODE NUMBER M IS IN RANGE OF STORED DATA  
14        IF(MM.LT.0) GO TO 300  
C  
C  
15        FOR POSITIVE M, WANT 0.LE.M.LE.(NBLADE-1)  
16        IF(0.LE.MM.AND.MM.LE.(NBLADE-1)) GO TO 310  
C  
C  
17        IF M POSITIVE BUT OUT OF RANGE, SUBTRACT INTEGER\*NBLADE  
C  
18        MTRIAL =MM  
19        NTRIAL=0  
20        CONTINUE  
21        NTRIAL=NTRIAL+1  
22        MSUM=MTRIAL-NTRIAL\*NBLADE  
23        IF(0.LE.MSUM.AND.MSUM.LE.(NBLADE-1)) GO TO 330  
24        GO TO 320  
25        330      MUSE=MSUM+1  
26        GO TO 340  
C  
C  
27        FOR NEGATIVE M, ADD INTEGER\*NBLADE TO M  
C  
28        340      MTRIAL=MM  
29        NTRIAL=0  
30        CONTINUE  
31        NTRIAL=NTRIAL+1  
32        MSUM=MTRIAL+NTRIAL\*NBLADE  
33        IF(0.LE.MSUM.AND.MSUM.LE.(NBLADE-1)) GO TO 360  
34        GO TO 350  
35        360      MUSE=MSUM+1  
36        GO TO 340  
C  
37        310      MUSE=MM+1  
C  
38        340      CONTINUE

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C  
C        WRITE(21,341) MM,MUSE  
341      FORMAT(' MM=',I5,' MUSE=',I5)  
C  
C        SEARCH HARMONIC ORDERS FOR FREQUENCY INTERPOLATION  
C  
C        WANT PMIN.LE.OMEGA.LE.PMAX  
C

IF(MM.LT.0) G1 TO 400  
NUPMIN=PSTART  
  
NUPMAX=PEND  
DO 10 P=PSTART,PEND-PSTEP,PSTEP  
IF (OMEGA.GE.(1.\*P)) NUPMIN=P  
10        CONTINUE  
DO 20 P=PEND,PSTART,-PSTEP  
IF (OMEGA.LT.(1.\*P)) NUPMAX=P  
20        CONTINUE  
GO TO 490

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C  
C        400        CONTINUE  
C  
C        FOR MODE NUMBER M.LT.0 MUST SHIFT FREQUENCY PARAMETER TO  
C        RETRIEVE CASCET DATA.  
C        EQUIV.(OMEGA)=OMEGA+ABS(MM)+MSUM

EQOMEG=OMEGA+IA3S(MM)+MSUM  
NUPMIN=PSTART  
NUPMAX=PEND  
DO 410 P=PSTART,PEND-PSTEP,PSTEP  
IF(EQOMEG.GE.(1.\*P)) NUPMIN=P  
410        CONTINUE  
DO 420 P=PEND,PSTART,-PSTEP  
IF(EQOMEG.LT.(1.\*P)) NUPMAX=P  
420        CONTINUE

C  
C        490        CONTINUE

C  
C        CONVERT TO FIND IP PARAMETER OF DATA STORAGE IN CASCET

IP=0  
DO 25 P=PSTART,PEND,PSTEP  
IP=IP+1  
IPP=P  
IF (NUPMIN.EQ.IPP) IPMIN=IP  
IF (NUPMAX.EQ.IPP) IPMAX=IP  
25        CONTINUE

C

```
21   WRITE(21,21) NUPMIN,NUPMAX  
      FORMAT(" NUPMIN=",I5," NUPMAX=",I5)  
      WRITE(21,22) IPMIN,IPMAX  
      FORMAT(" IPMIN=",I5," IPMAX=",I5)
```

C

C

```
C KILL PROGRAM IF DESIRED FREQUENCY IS OUT OF RANGE OF DATA  
PSTARF=FLOAT(PSTART)  
PENDF=FLOAT(PEND)  
OMEGAT=OMEGA  
IF (MM.LT.0) OMEGAT=E20M88  
IF(PSTARF.LE.OMEGAT.AND.OMEGAT.LE.PENDF) GO TO 343  
      WRITE(5,342)  
342   FORMAT(" FREQUENCY OUT OF RANGE OF DATA FILE")  
      STOP  
343   CONTINUE
```

C

C

```
118   XSIGN=1.
```

C

```
C***** RETURN TO LINE (111) TO REPEAT FOR DOWNSTREAM  
C PROPAGATION *****
```

C

```
111   CMNS=(MT*MA*OMEGA+XSIGN*K4NS)/BETASQ
```

C

C INITIALIZE VARIABLES

C ISUMR IS ERROR CODE ACCUMULATOR FOR BESSEL WEIGHTING FUNCTION  
C PMNS IS RESULT OF DOUBLE INTEGRAL  
C SWTR IS WEIGHTING SIGN FUNCTION FOR RADIAL INTEGRATION

C

```
PMNS=0.  
DELTAR=(1.-SIGMAR)/(NRADNJ-1)  
ISUMR=0  
IDAT=2
```

C

```
SWTR=-1.
```

C

```
C***** START RADIAL INTEGRATION LOOP HERE *****
```

C

```
DO 901 IRNU=1,NRADNU
```

C

C

C

RADIAL POSITION SEARCH FOR INTERPOLATION COORDINATES

C

C

```
WANT RR(IRMIN).LE.RRNU(IRNU).LE.RR(IRMAX)  
***NOTE: RR(1)=RRNU(1)  
RR(NRAD)=RRNU(NRADNU)
```

C  
C  
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```
IF (IRNU.EQ.1) GO TO 50
IF (IRNU.EQ.NRADNU) GO TO 60
IRMIN=1
IRMAX=NRAD
DO 30 IR=1,NRAD-1,1
    IF (RRNU(IRNU).GE.RR(IR)) IRMIN=IR
30  CONTINUE
DO 40 IR=NRAD,1,-1
    IF (RRNU(IRNU).LT.RR(IR)) IRMAX=IR
40  CONTINUE
GO TO 70
50  CONTINUE
    IRMIN=1
    IRMAX=2
GO TO 70
60  CONTINUE
    IRMIN=NRAD-1
    IRMAX=NRAD
GO TO 70
70  CONTINUE
```

```
C  
C  
    WRITE(21,71) IRMIN,IRMAX
71   FORMAT(" IRMIN=",I5," IRMAX=",I5)
    WRITE(21,72) RR(IRMIN),RRNU(IRNU),RR(IRMAX)
72   FORMAT(" RR(IRMIN=",E10.4," RRNU(NU=",E10.4," RR(IRMAX=",E10.4)
```

```
C  
C  
BLADE GEOMETRY AT RADIAL STATION OF INTEGRATION
R=RRNU(IRNU)
IF(R.LE.VGEOM(IDAT,1)) GO TO 201
IDAT=IDAT+1
IF(IDAT.GT.NDAT) IDAT=NDAT
201  DELTA=(R-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
DO 210 IX=2,3
210  XX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))
```

```
C  
C  
B=XX(1)/2.
CHI=XX(2)
7010  WRITE(21,7010) B,CHI,R
    FORMAT(" B=",E10.4," CHI=",E10.4," R=",E10.4)
```

```
C  
C  
COSCHI=COS(CHI)
SINCHI=SIN(CHI)
```

```
C  
C  
ZMOD=SIGMAC*B*(GMNS*COSCHI+MM*SINCHI/R)
```



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C STATION

C NOTE THAT Z=I\*\*IKOUNT BELOW

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```
RRRS=(0.,0.)
Z=(1.,0.)
DO 5000 IKOUNT=0,NCHORD
BM=1.
IF(IKOUNT.EQ.0.OR.IKOUNT.EQ.NCHORD) BM=0.5
ARGU=IKOUNT*IZ*PI/NCHORD
IF(IKOUNT.GT.0) GO TO 5010
RRS=BM*Z*B0
GO TO 5020
5010 CONTINUE
RRS=BM*Z*B0(IKOUNT)*COS(ARGU)
5020 CONTINUE
Z=Z*I
RRRS=RRRS+RRS
5030 CONTINUE
RRRS=RRRS*2.*PI/NCHORD
BN=1.
IF(IZ.EQ.NCHORD) BN=0.5
```

C

C INTERPOLATE PRESSURE VALUES IN FREQUENCY AND RADIUS

```
MCOUNT=MUSE
Y=(1.-PP)*(1.-QQ)*CASSET(IZ,IRMIN,MCOUNT,IPMIN)
Y=Y+PP*(1.-QQ)*CASSET(IZ,IRMAX,MCOUNT,IPMIN)
Y=Y+QQ*(1.-PP)*CASSET(IZ,IRMIN,MCOUNT,IPMAX)
Y=Y+PP*QQ*CASSET(IZ,IRMAX,MCOUNT,IPMAX)
```

```
WRITE(21,2) CASSET(IZ,IRMIN,MCOUNT,IPMIN)
WRITE(21,2) CASSET(IZ,IRMAX,MCOUNT,IPMIN)
WRITE(21,2) CASSET(IZ,IRMIN,MCOUNT,IPMAX)
WRITE(21,2) CASSET(IZ,IRMAX,MCOUNT,IPMAX)
```

2 FORMAT(" CASSET=",2E10.4)

C EVALUATE FINITE CHORDWISE SUM TO APPROX. INTEGRAL

```
QMNST=Y*RRRS*BN
QMNS=QMNS+Y*RRRS*BN
5030 WRITE(21,5030) IZ,QMNST
FORMAT(" IZ=",I5," QMNST=",2E10.4)
220 CONTINUE
```

C \*\*\*\*\*END OF CHORDWISE INTEGRATION LOOP (220) \*\*\*\*\*

```
7022 WRITE(21,7022) IRNU,QMNS
FORMAT(" IRNU=",I3," QMNS=",2E10.4)
```

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8010 CONTINUE  
GO TO 8013  
8012 CONTINUE  
SUMNU=0.  
8013 CONTINUE  
WRITE(21,8015) SUMNU,P,TURM  
8015 FORMAT(" SUMNU=",E10.4," P=",I5," TURM=",E10.4)

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C  
C  
C  
FMNS=CB\*CC\*CD\*SUMNU/R  
C  
C

WHTR=1.+SWTR/3.  
SWTR=-SWTR  
IF(IR.EQ.1.OR.IR.EQ.NRAD) WHTR=WHTR/2.

C  
C  
PMNS=PMNS+WHTR\*FMNS\*DELTAR\*SIGHAC\*SIGHAC\*2.  
WRITE(21,7016) PMNS  
7016 FORMAT(" PMNS SUM(R)=",E10.4)  
901 CONTINUE

C\*\*\*\*\* END OF RADIAL INTEGRATION LOOP (901) \*\*\*\*\*  
C  
C  
C

SMN=((BETAS2\*NBLADE)\*\*2)\*MA\*MT\*OMEGA\*PMNS/PI/KMNS  
SMN=SMN/(1.-SIGMAR\*\*2)/(OMEGA\*MT\*XIGN\*MA\*KMNS)\*\*2  
SMN=-XIGN\*SMN

C  
C  
MULTIPLY OUTPUT BY 2 (ADDS +3DB) TO ACCOUNT FOR ENERGY  
C IN NEGATIVE FREQUENCY  
SMN=SMN\*2.

C  
RELPWR=SMN  
IPWR=1  
IF(RELPWR.EQ.0.) GO TO 915  
RELPRL=10.\*ALJG10(ABS(RELPWR))  
GO TO 920  
915 IPWR=0  
920 CONTINUE

C  
C  
C  
IP(XSIGN.LT.0.) GO TO 9800

C  
C  
3000 WRITE(5,3000)  
FORMAT("UPSTREAM ")  
WRITE(5,8101) GMNS

C <MTHEOBALD>INTURB.FOR;40 Mon 29-Sep-80 10:13AM PAGE 1:10

```
8101  FORMAT(" GAMMA M,N,SB =",E16.8)
      WRITE(5,8102) SMN
  8102  FORMAT(" REL. MODAL SOUND POWER SPECTRAL DENSITY=",E10.4)
      WRITE(5,8500) IER
      WRITE(5,5500) ISUMR
  8500  FORMAT(" SUM OF ALL ERRORS IN PSI CALCULATIONS =",I5)
      IF(IPWR.EQ.0) GO TO 970
      WRITE(5,3600) RELPRL
      GO TO 980
  970   CONTINUE
      WRITE(5,952)
  980   CONTINUE
  8600  FORMAT(" REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=",E10.4)
      WRITE(21,7200)
  7200  FORMAT(" END OF UPSTREAM INTEGRATION")
      XSIGN=-1.
      SPWR(1)=RELPWR
      GO TO 111
```

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```
C
C***** RETURN TO LINE 111 TO COMPUTE DOWNSTREAM PROPAGATION
C*****
C
 9900  WRITE(5,8200)
 8200  FORMAT("DOWNSTREAM")
      WRITE(5,8201) GMNS
  8201  FORMAT(" GAMMA M,N,SB =",E16.8)
      WRITE(5,8202) SMN
  8202  FORMAT(" REL. MODAL SOUND POWER SPECTRAL DENSITY=",E10.4)
      WRITE(5,8400) IER
      WRITE(5,5500) ISUMR
  5500  FORMAT(" SUM OF ALL ERRORS IN RS CALCULATIONS =",I5)
  8400  FORMAT(" SUM OF ALL ERRORS IN PSI CALCULATIONS =",I5)
      IF(IPWR.EQ.0) GO TO 950
      WRITE(5,8500) RELPRL
      GO TO 960
  950   CONTINUE
      WRITE(5,952)
  952   FORMAT(" SOUND POWER SPECTRAL DENSITY FOR MODE=0/UNEXCITED")
  960   CONTINUE
      SPWR(2)=RELPWR
      WRITE(21,7202)
  7202  FORMAT(" END OF DOWNSTREAM INTEGRATION")
      RETURN
      END
```

## **PROGRAM MAINTW**

**This is a calling program to  
control the computation of  
pressure data for the wake  
turbulence case.**

```
PROGRAM MAINTW
DIMENSION IDATA(10),RDATA(20),VGEOM(10,7)
DIMENSION VELOCV(10,2)
REAL MT,MA,MUV,LX,LR,LTHETA
INTEGER PSTART,PEND,P,PRANGE,PSTEP
DATA (IDATA(J),J=1,10)/10*0/
DATA (RDATA(J),J=1,20)/20*0.0/
```

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#### ROTOR WAKE TURBULENCE-STATOR INTERACTION---MATRIX STORAGE

THIS PROGRAM GROUP CALCULATES AND STORES VECTORS OF  
THE COMPLEX PRESSURE DISTRIBUTION ACROSS THE STATOR VANE.

DATA REQUIRED TO EXECUTE THIS ROUTINE INCLUDE:

1. VANE GEOMETRY
2. ROTOR OPERATING SPEEDS
3. NUMBER OF RADIAL AND CHORDWISE POSITIONS AT WHICH THE  
PRESSURES ARE CALCULATED
4. FREQUENCY RANGE OF INTEREST (EXPRESSED IN TERMS  
OF HARMONIC ORDER OF SHAFT ROTATION).

THE RANGE OF CIRCUMFERENTIAL MODE NUMBER M IS 0 TO NVANE-1.

CHORD MUST BE NO GREATER THAN 20.

```
1501  FORMAT(G20.8)
      WRITE(5,2001)
2001  FORMAT(" NVANE=")
      READ(5,1001) NVANE
      WRITE(5,2101) NVANE
2101  FORMAT(" NVANE=",I3)
      WRITE(5,2002)
2002  FORMAT(" NBLADE=")
      READ(5,1001) NBLADE
      WRITE(5,2102) NBLADE
2102  FORMAT(" NBLADE=",I3)
      WRITE(5,2003)
2003  FORMAT(" HUB RADIUS DIVIDED BY DUCT RADIUS =")
      READ(5,1001) SIGMAR
      WRITE(5,2103) SIGMAR
2103  FORMAT(" SIGMAR=",E16.8)
      WRITE(5,2004)
2004  FORMAT(" VANE TIP CHORD DIVIDED BY DUCT RADIUS=")
      READ(5,1001) SIGMAC
      WRITE(5,2104) SIGMAC
2104  FORMAT(" SIGMAC=",E16.8)

      WRITE(5,2006)
```

C <MTHEOBALD>MAINTW.FOR;3 Sun 21-Sep-80 3:58PM PAGE 1:1

```

2006 FORMAT(' NDAT =')
READ(5,1001) NDAT
WRITE(5,2106) NDAT
2106 FORMAT(' NDAT= ',I3)
WRITE(5,2007)
2007 FORMAT(' VANE GEOMETRY MATRIX INPUT')
WRITE(5,2008)
2008 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')

C
C
2009 DO 10 IROW=1,NDAT
      WRITE(5,2009) IROW
      FORMAT(' ROW= ',I3,' R/RDUCT =')
      READ(5,1001) VGEOM(IROW,1)
      WRITE(5,2010)
2010 FORMAT(' C/CTIP =')
      READ(5,1001) VGEOM(IROW,2)
      WRITE(5,2011)
      FORMAT(' THETA (DEGREES)=')
      READ(5,1001) VGEOM(IROW,3)
      VGEOM(IROW,3)=VGEOM(IROW,3)*.0174533
      CONTINUE

10
C
C
2020 WRITE(5,2020)
      FORMAT(' VANE GEOMETRY MATRIX IS')
      DO 11 IROW=1,NDAT
      WRITE(5,2120) (VGEOM(IROW,ICOLUMN),ICOLUMN=1,3)
      11 FORMAT(' ',7E10.3)
      CONTINUE

C
C
2120
      WRITE(5,5000)
      FORMAT(' TYPE 1 TO INPUT ROTOR WAKE VELOCITY; 0 FOR FREE
      1 VORTEX')
      READ(5,1001) IVOR
      WRITE(5,5010) IVOR
      5010 FORMAT(' IVOR= ',I3)
      IF (IVOR.EQ.0) NVELO=0
      IF (IVOR.EQ.0) GO TO 4005

C
C
3000 WRITE(5,3000)
      FORMAT(' NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=')
      READ(5,1001) NVELD
      WRITE(5,3002) NVELO
      3002 FORMAT(' NVELD= ',I3)
      WRITE(5,3004)
      3004 FORMAT(' INPUT MATRIX FOR MEAN ROTOR FLOW')
      WRITE(5,3006)

```

C <MTHEOBALD>MAINTN.FOR;3 Sun 21-Sep-80 3:58PM PAGE 1:2

```
3006 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
DO 4000 IROW=1,NVELO
WRITE(5,3008) IROW
3008 FORMAT(' ROW=',I3,' R/RDUCT=')
READ(5,1001) VELOCV(IROW,1)
WRITE(5,3012)
3012 FORMAT(' MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U
1 AXIAL0=")
READ(5,1001) VELOCV(IRUW,2)
4000 CONTINUE
C
C
3014 WRITE(5,3014)
FORMAT(' MEAN ROTOR FLOW VELOCITY MATRIX IS')
DO 4002 IROW=1,NYELD
WRITE(5,3016) (VELOCV(IROW,ICOLUMN),ICOLUMN=1,2)
3016 FORMAT(' ',2E10.4)
4002 CONTINUE
C
C
4005 CONTINUE
C
C
C
2030 WRITE(5,2030)
FORMAT(' MT =')
READ(5,1001) MT
WRITE(5,2130) MT
2130 FORMAT(' MT=',E16.8)
WRITE(5,2031)
2031 FORMAT(' MA =')
READ(5,1001) MA
WRITE(5,2131) MA
2131 FORMAT(' MA =',E16.8)
C
C
C
C
IF(IVOR.EQ.1) GO TO 6000
2032 WRITE(5,2032)
FORMAT(' VYFM/VXM @ R=RDUCT=')
READ(5,1001) MUV
WRITE(5,2132) MUV
2132 FORMAT(' MUV=',E10.4)
6000 CONTINUE
IF (IVOR.EQ.1) MUV=0.
C
C
C
WRITE(5,2035)
```

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```
2035 FORMAT(" NUMBER OF RADIAL STATIONS =")  
      READ(5,1001) NRAD  
      WRITE(5,2135) NRAD  
2135 FORMAT(" NRAD=",I4)  
      WRITE(5,2036)  
2036 FORMAT(" NUMBER OF CHORDWISE STATIONS (.LE.20) =")  
      READ(5,1001) NCHORD  
      WRITE(5,2136) NCHORD  
2136 FORMAT(" NCHORD=",I4)  
C  
C  
      WRITE(5,100)  
100 FORMAT(" START FREQUENCY(HARMONIC NO. OF SHAFT) =")  
      READ(5,1001) PSTART  
      WRITE(5,110) PSTART  
110 FORMAT(" PSTART=",I4)  
      WRITE(5,120)  
120 FORMAT(" END FREQUENCY(HARMONIC NO. OF SHAFT) =")  
      READ(5,1001) PEND  
      WRITE(5,130) PEND  
      FORMAT(" PEND=",I4)  
C  
C  
      WRITE(5,140)  
140 FORMAT(" FREQUENCY STEP SIZE (HARMONIC ORDERS) =")  
      READ(5,1001) PSTEP  
      WRITE(5,150) PSTEP  
150 FORMAT(" PSTEP=",I4)  
      PANGE=(PEND-PSTART)/PSTEP+1  
      IDATA(1)=NVANE  
      IDATA(2)=NBLADE  
      IDATA(3)=NRAD  
      IDATA(4)=NCHORD  
      IDATA(5)=NDAT  
      IDATA(6)=PSTART  
      IDATA(7)=PEND  
      IDATA(8)=PSTEP  
      IDATA(9)=IVOR  
      IDATA(10)=NVELO  
  
C  
C  
      RDATA(1)=MT  
      RDATA(2)=MA  
      RDATA(4)=SIGMAC  
      RDATA(5)=SIGMAR  
      RDATA(6)=MUV  
  
C  
C  
      CALL STATOR(IDATA,RDATA,VGEOM,VELOCY)  
      STOP  
      END
```

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## **PROGRAM STATOR**

**Program calculates and stores the pressures generated on a turbofan stator by wake turbulence.**

SUBROUTINE STATOR(IDATA,RDATA,VGEOM,VELOCV)

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DIMENSION OF DELTAP=20

DIMENSION OF CASCET=(NCHORD,NRAD,NVANE,PRANGE)

NOTE NCHORD MUST BE NO GREATER THAN 20

DIMENSION DELTAP(20)

DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6)

DIMENSION CASCET(3,5,11,3)

DIMENSION A(72),VELOCV(10,2)

REAL KB,MR,MA,MT,MV4,MTHETA

COMPLEX I,DELTAP,CASCET

INTEGER PSTART,PEND,P,PRANGE,PSTEP

I=(0.,1.)

PI=3.1415926

NVANE=IDATA(1)

NBLADE=IDATA(2)

NRAD=IDATA(3)

NCHORD=IDATA(4)

NDAT=IDATA(5)

PSTART=IDATA(6)

PEND=IDATA(7)

PSTEP=IDATA(8)

IVOR=IDATA(9)

NVELO=IDATA(10)

WRITE(5,160)

160 FORMAT(\* ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)\*)

READ(5,1003) A

1003 FORMAT(72A1)

MT=RDATA(1)

MA=RDATA(2)

SIGMAC=RDATA(4)

SIGMAR=RDATA(5)

IDAT=2

IDOT=2

START LOOPS TO CALL CASC--BEGIN WITH LOOP ON RADIAL  
POSITION TO MINIMIZE INTERPOLATION.

DO 308 IR=1,NRAD

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DO 308 P=PSTART,PEND,PSTEP  
IP=IP+1

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OMEGBC=MT\*SIGHMAC\*B\*B

MR=(MA\*\*2+MTTHETA\*\*2)\*\*.5

KB=MT/MR\*B\*SIGHMAC\*B  
SIGMA=-2.\*PI\*MM/NVANE

H=2.\*PI\*R/NVANE/SIGHMAC/B

ANGLE= -THETA

300 WRITE(21,300)  
FORMAT("BINPUT TO SUBROUTINE CASC")  
302 WRITE(21,302) OMEGBC  
FORMAT(" OMEGBC=",E10.4)  
WRITE(21,304) MR,KB,SIGMA  
304 FORMAT(" MR=",E10.4," KB=",E10.4," SIGMA=",E10.4)  
WRITE(21,306) H,ANGLE,NCHORD  
306 FORMAT(" H=",E10.4," ANGLE=",E10.4," NCHORD=",I3)

CALL CASC(OMEGBC,MR,KB,SIGMA,H,ANGLE,NCHORD,DELTAP,IERP)

STORE RESULTS OF CASC IN STORAGE MATRIX FOR DISK FILE.  
MATRIX POSITION DESCRIPTORS ARE (IN ORDER OF APPEARANCE):  
1. CHORDWISE POSITION (TRAILING TO LEADING EDGES)  
2. RADIAL POSITION (INNER RADIUS TO OUTER RADIUS)  
3. CIRCUMFERENTIAL MODE NUMBER + 1 (M+1)  
4. ORDER OF FREQUENCY COMPUTATIONS (FIRST TO LAST)  
WITH: IP=1 FOR PSTART  
IP=PRANGE FOR PEND

DO 310 ICK=1,NCHORD  
CASCET(ICK,IR,MCOUNT,IP)=DELTAP(ICK)

C <MTHEOBALD>STATOR.FOR;9 Mon 22-Sep-86 4:13PM PAGE 1:3

```
310    CONTINUE
      WRITE(5,7500) IERP
7500    FORMAT(" ERROR CODE FROM INVERSION ROUTINE=",I3)
      WRITE(21,7025)
7025    FORMAT(" OUTPUT FROM CASC:(DELTAP(IQ),IQ=1,NCHORD")
      WRITE(21,7002) (DELTAP(IQ),IQ=1,NCHORD)
7002    FORMAT(5X,6E10.4)
```

C

C

C

C

308 CONTINUE

C

C STORE MATRIX OF PRESSURE VALUES ON THE DISK FOR LATER
C PROCESSING BY OTHER PROGRAMS.

C

```
CALL OPILE(23,"STAT")
      WRITE (23) A
      WRITE (23) IDATA
      WRITE (23) RDATA
      WRITE (23) VGEOM
      WRITE (23) VELOCV
      WRITE (23) CASCET
```

C

C

ENDFILE 23

C

C

STOP
END

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**PROGRAM WASXCH**

Program determines which modes propagate for the case of rotor wake turbulence and controls the noise computation.

**PRECEDING PAGE BLANK NOT FILMED**

```
PROGRAM ASKCH
DIMENSION CASSET(8,5,11,3)
DIMENSION ICA(8),IDATA(12)
DIMENSION RDATA(22),VGEDM(13,7),POWER(2),SWR(2),RELPR(2)
DIMENSION NPCDA(4),VELOCV(13,2)
DIMENSION A(72)
DIMENSION ISUMTO(123)
COMPLEX CASSET
REAL LA,LH,LTHETA
INTEGER PRANGE,PSTART,PSTEP,PEND
REAL ME,MA

C
      DATA(ISUMTO(J),J=1,123)/100*#/
      DATA(PU+PR(J),J=1,2)/2*3.#
C
```

C CALLING PROGRAM FOR PURPOSES TO SEARCH OUT AND CALCULATE  
C ALL PROPAGATING MODES AT A GIVEN POSITIVE FREQUENCY.

C OPEN FILE "STAT" AND READ INPUT ARRAYS
C INCLUDING MAIN STORAGE MATRIX "CASSET"

C\*\*\*\*\*NOTE THAT "STAT" IS A SEQUENTIAL UNFORMATTED BINARY FILE--  
C  
C ORDER OF STORAGE=A, IDATA, RDATA, VGEDM, VELOCV, CASSET
C\*\*\*\*\*

```
C
      CALL FILE(23,"STAT")
      READ(23) A
      READ(23) IDATA
      READ(23) RDATA
      READ(23) VGEDM
      READ(23) VELOCV
      READ(23) CASSET
      ENDFILE 23
```

C
 WRITE(5,0)
 5 FORMAT(" USER-ASSIGNED TITLE OF DATA SET FROM FILE \"STAT\" IS")
 WRITE(5,0) A
 6 FORMAT(" ",72A1)

PSTART=IDATA(5)
PEND=IDATA(7)
PSTEP=IDATA(8)
PRANGE=(PEND-PSTART)/PSTEP+1
NPCON(1)=PSTART
NPCON(2)=PEND
NPCON(3)=PSTEP
NPCON(4)=PRANGE

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C  
C  
C     ENTER NOISE FREQUENCY OF INTEREST(MUST BE POSITIVE FREQUENCY)  
C

1001 FORMAT(624.8)  
WRITE(5,112)  
110 FORMAT(" NOISE FREQUENCY/SHAFT FREQUENCY=")  
READ(5,1101) DMEGA  
RDATA(5)=DMEGA  
115 FORMAT(" DMEGA=",E12.4)  
WRITE(5,115) RDATA(5)

C  
C     SELECT NO. OF RADIAL POSITIONS TO INTERPOLATE PRESSURES  
C     (ASSUMED THAT NRADNU.GE.NRAD)  
C

C\*\*\*\*\*NOTE: NRADNU MUST BE .LE.30 UNLESS DIMENSION STATEMENTS IN  
C                 "NRADNU" ARE TO BE SUBSTITUTED  
C\*\*\*\*\*

120 WRITE(5,122)  
FORMAT(" NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=")  
READ(5,1221) NRADNU  
RDATA(13)=FLURT(NRADNU)  
WRITE(5,132) NRADNU  
130 FORMAT(" NRADNU=",14)  
WRITE(5,2337)  
2237 FORMAT(" ACCURACY OF BESSSEL FLS=")  
READ(5,1231) E3  
WRITE(5,2137) E3  
2137 FORMAT(" E3=",E12.4)  
WRITE(5,238)  
2238 FORMAT(" ACCURACY OF CONVERGENCE TO ROOT XNS=")  
READ(5,1231) EC  
WRITE(5,2134) EC  
2134 FORMAT(" EC=",E12.4)

C  
C     ENTER TURBULENCE CHARACTERISTICS

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2033 FORMAT(" AND ALPH=")  
READ(5,1031) WIDTH  
WRITE(5,2133) WIDTH  
2133 FORMAT(" WIDTH=",E12.4)  
WRITE(5,2134)  
2034 FORMAT(" TURBULENCE INTENSITY(RMS FLUCTUATING U/U BAR)=")  
READ(5,1031) EPSN  
2134 FORMAT(" EPSN=",E12.4)  
WRITE(5,2134) EPSN

C  
0810 WRITE(5,610)  
FORMAT(" TURBULENCE LENGTH SCALE IN AXIAL DIRECTION=")  
READ(5,1231) LX  
WRITE(5,612) LX

```

0002 FORMAT( " LX=",E14.4)
WRITE(5,002)
0004 FORMAT( " TURBULENCE LENGTH SCALE IN RADIAL DIRECTION=")
READ(5,101) LR
WRITE(5,0025) LR
0006 FORMAT( " L0=",E14.4)
WRITE(5,0028)
0008 FORMAT( " TURBULENCE LENGTH SCALE IN CIRCUMFERENTIAL DIRECTION=")
READ(5,101) LTTHETA
WRITE(5,0011) LTTHETA
0010 FORMAT( " LTTHETA=",E14.4)
READ(5)=EPSA
RDATA(7)=SIGMTH
RDATA(15)=LA
RDATA(16)=LN
READ(17)=LTHETA
READ(9)=ES
RDATA(18)=BC
M1=RDATA(1)
MA=READ(2)
SIGMAF=0.75*TA(5)

```

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$$X_{\text{eff}} = \min(1, 1/(1.0 - 44^{\alpha} \cdot 2)^{0.5})$$

$\alpha = 1$  T<sub>0</sub>(2*i*, 2*i*-1) Xv4K

«ДАМТИ» КОМПАНИЯ ПОД ПРЕДСТАВЛЕНІЯМ = 15.3)

START WITH PLANE WAVE MODE (0,0). COUNT UP IN N, THEN M UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

J=1  
v=4

RESTART & COUNT HERE FOR SET 4

四

## INCREMENT N

n = n<sub>i</sub>

$S_A + S = 14 \pm 5$  (")

C  
C  
C

CALL ANRT (MARS,S,SIGMAR,AM,SC,X4A,IcS,IcC)

C  
C  
C

IF MODE IS CUT OFF, GO TO 680J

IF(AMN.GE.XMAX) GO TO 677J

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C

```
3048 = WRITE(21,3803)
      READ(MAT,"MODE DATA")
      WRITE(21,381) OMEGAN,M,N,X4A
      381 FORMAT("OMEGA=",1F.4," M=",13," N=",13," X4A=",13.4)
      IF(XAN.EQ.0.) GO TO 1200
      CONPRA=XMAX/X4A
      WRITE(21,400) CONPRA
      400 FORMAT("CUTOFF RATIO FOR m=0=",E17.4)
      GO TO 1275
```

C

CONTINUE

C

```
4035 FORMAT("PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE")
1000 CONTINUE
```

C

```
4035 FORMAT("PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE")
```

C

CONTINUE

C

```
3062 WRITE(21,3042) IcB
      READ(MAT,"SUM OF BESSEL FUNCTION ERROR CODES =",I3)
      WRITE(21,3043) IcC
      3043 FORMAT("ERROR CODE FOR CONVERGENCE TO ROOT AMN =",I3)
```

C

C

NORMALIZE MODE AMPLITUDE

C

CALL SIGMA (MARS,SIGMAR,AMN,AMN,BMN,BP,IcR)

C

C

```
3024 WRITE(21,3144) AMN,RMN
      READ(MAT,"AMN =",130.8," RMN =",130.8)
      WRITE(21,3245) IcR
      3245 FORMAT("ERROR CODE FOR BESSEL FUN IN AMN AND BMN CALC =",I12)
```

C

C

```
RDATA(11)=AMN
RDATA(12)=AMN
RDATA(13)=RMN
IDATA(0)=0
IDATA(7)=0
```

C

C

```
1 CALL MATUR(1U3TK,RDATA,VGUM,VLLUC,SPWR,CASGET,HPGUM,
     1 IUMTU)
     1 P04ER(1)=POWER(1)+SPWR(1)
     1 P04ER(2)=POWER(2)+SPWR(2)
```

C <MTHEODALD>.AS<CH.0K;7 FRI 12-DEC-84 1:46PM PAGE 1:4

C  
C  
C DO NOT SWITCH SIGN OF A IF M=2  
C  
C IF(M.EQ.2) GO TO 22  
C  
C IUDATA(0)=IUDATA(5)  
C  
C WRITE(21,8389) IDATA(5),IDATA(7),RDATA(3)  
3382 FORMAT("M=",ID," N=",N," DMAX=",E10.4)  
C  
C SWITCH SIGN OF A AND RECALCULATE  
C  
C CALL MATURD(IDATA,RDATA,NDIM,NBLUDR,SPNR,CACCF,RCUNS,  
1 ISUATO)  
POWER(1)=POWER(1)+SPWR(1)  
POWER(2)=POWER(2)+SPWR(2)  
C  
C IDATA(5)=IUDATA(0)  
C  
C GO TO 22  
C  
C  
C  
C IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.  
C  
C 6080 IF(N.EQ.1) GO TO 781?  
C  
C  
C N=MAX=N-1  
C WRITE(21,5671) MAX  
6881 FORMAT("LARGEST PROPAGATING N FOR THIS A =",ID)  
C  
C J=J+1  
C  
C INCREMENT N  
C  
C M=N+1  
C GO TO 15  
C  
C  
C N=1 TO REACH THIS POINT  
7880 CONTINUE

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C  
C

WITE(21,781)  
7001 FORMAT(" NO MORE PROPAGATING MODES FOR THIS OMEGA")  
10 CONTINUE  
WITE(5,981)  
9001 FORMAT(" PROBLEM COMPLETE")  
DO 500 JJ=1,2  
18(PJ=2\*(JJ)+1,2,7) GO TO 5215  
RELPK(JJ)=10.\*ALUG1\*(ABS(POWER(JJ)))  
GO TO 557  
5215 RELPK(JJ)=1.e+30.  
CONTINUE  
IF(ELP(1).EQ.1.e+35) GJ TO 5315  
WITE(5,610) RELPK(1)  
GO TO 500  
5315 WITE(5,5510)  
5010 FORMAT(" FREQUENCY IS CUT OFF")  
600 CONTINUE  
510 FORMAT(" RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=",E10.4)  
IF(RELPK(2).EQ.1.e+35) GJ TO 5415  
WITE(5,630) RELPK(2)  
GJ TO 527  
5415 WITE(5,5510)  
528 CONTINUE  
630 FORMAT(" REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=",E10.4)  
STOP  
END

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## **PROGRAM WATURB**

**Program computes the sound power  
generated by a turbofan stator  
subjected to wake turbulence.**

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SUBROUTINE NATURH(IDATA,RDATA,VGEOM,VELOCV,SPWR,CASCET,NPCON,  
1 ISUMTU)

PROGRAM COMPUTES THE SOUND POWER GENERATED BY A TURBOFAN  
STATOR SUBJECTED TO INLET TURBULENCE. THIS IS A SIMPLIFIED  
VERSION SUITABLE FOR VERY SMALL TURBULENCE LENGTH SCALES  
IN THE RADIAL DIRECTION

PROGRAM INTERPOLATES IN RADIAL POSITION AND FREQUENCY FROM A  
STORED MATRIX OF PRESSURE DISTRIBUTIONS (NAME=CASCET)

```
DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6),IERPSI(2),SPWR(2)
DIMENSION BJ(20)
DIMENSION PSISTO(30),NPCON(4),RR(30),RRNU(30)
DIMENSION VELOCV(10,2)
DIMENSION CASCET(8,5,11,3)
DIMENSION ISUMTD(100),SUMIJT(100,30)
INTEGER P,PSTEP,PRANGE,PSTART,PEND,S1
REAL KMNS,MR,MT,MA,LR,LTHETA,LX,MYM,MTHETA
COMPLEX I,QMNS,A1,CASCET
COMPLEX L,RRS,RRRS,MMST
COMPLEX X
```

\*\*\*\*\*  
C DIMENSION OF PSISTU AND RRNU MUST BE .GE. NRAUNU

C DIMENSION OF RR MUST BE .GE. NRAD

\*\*\*\*\*  
I=(0.,1.)  
PI=3.1415926

```
NRAUNU=IFIX(RDATA(15))
NVAHE=IDATA(1)
NULAD=IDATA(2)
NRAU=IDATA(3)
NCHUMU=IDATA(4)
NDAT=IDATA(5)
MM=IDATA(6)
NN=IDATA(7)
IVUR=IDATA(9)
NVELO=IDATA(10)
UMEGA=RDATA(8)
PRANGE=NPCON(4)
PSTART=NPCON(1)
PEND=NPCON(2)
PSTEP=NPCON(3)
SIGMAR=RDATA(5)
```

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PAGE 1 of 1

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```

      WRITE(5,6320) MM,NN,OMEGA
8300    FORMAT('MM=',I5,'   NN=',I5,'   OMEGA=',E15.4)
7204    FORMAT(' NRAD=',I3,' NHDRU=',I3)

```

LIST NONDIMENSIONAL RADIAL POSITIONS AVAILABLE IN STORED  
DATA (NEEDED FOR INTERPOLATION)

```

DO 5 IR=1,NRAD
R=SIGMAR+(IR-1.)*(1.-SIGMAK)/(NRAD-1.)
RR(IR)=R
CONTINUE

```

```
FORMAT(' R VALUES FROM STORAGE ARE')  
FORMAT(7E10.4)
```

```

MT=RDATA(1)
MA=RDATA(2)
EPSW=RDATA(3)
SIGNAC=RDATA(4)
MUV=RDATA(5)
WWIUTM=RDATA(7)
EDG=RDATA(9)
EC=RDATA(10)
XMN=RDATA(11)
AMN=RDATA(12)
BMN=RDATA(13)
LX=RDATA(15)
LR=RDATA(15)
LTHTA=RDATA(17)

```

INITIALIZE ERROR CODE ACCUMULATOR IN PSI COMPUTATIONS  
IEK=3

**LIST NONDIMENSIONAL RADIAL POSITIONS TO BE USED IN INTERPOLATION**

DU = 7 IRNU=1, NRAUNU  
 R=SIGMAR+(IRNU-1.)\*(1.-SIGMAR)/(NRAUNU-1.)  
 IRNU(IRNU)=R

**COMPUTE AND STORE MODE SHAPES WEIGHTING AT EACH RADIUS**

C  
C  
ARG=XMN\*R  
CALL RMODE(MM,ARG,AMN,SMN,PSI,EB,IERSI)  
PSISTO(IRNU)=PSI  
IER=IER+IERSI(1)+IERSI(2)  
CONTINUE  
C  
C  
9 FORMAT(" R VALUES FOR INTERPOLATION ARE")  
11 FORMAT(" PSISTO VALUES ARE")  
C  
C PERFORM SUMMATION OVER TRANSFORMS OF AUTOCORRELATION  
C FUNCTIONS FOR LATER USE. THIS SUMMATION IS A  
C FUNCTION OF MODE NUMBER M AND RADIUS R FOR A GIVEN SET  
C OF INPUT PARAMETERS.  
C  
C CHECK TO SEE WHETHER SUM IS AVAILABLE FROM STORAGE  
C  
C MINDEX=MM+50  
IF(ISUMTO(MINDEX).EQ.1) GO TO 6040  
C  
C MAKE SURE STORAGE LIMITS ARE NOT EXCEEDED  
C  
6010 IF(MM.GT.49) WRITE(5,5010)  
FORMAT(" MODE NUMBER M EXCEEDS STORAGE OF MATRIX SUMTOT")  
IF(MM.GT.49) STOP  
C  
C COMPUTE SUMMATION AS A FUNCTION OF R AND STORE IN SUMTOT  
C  
DO 6020 IRNU=1,NRADNU  
R=RRNU(IRNU)  
SUMTUT(MINDEX,IRNU)=P.  
C  
C LIMITS ON DOUBLE SUM ADAPT TO PHYSICAL PARAMETERS  
C  
MM1MAX=INT(23.\*R/NBLADE/NNIDTH)  
MW1MAX=INT(1./NVANE\*(16.\*R/LTHETA+MM1MAX\*NBLADE+20.))  
DO 6022 MM1=-MM1MAX,MM1MAX  
FARG=MM1\*NBLADE\*NNIDTH/R  
PHIARG=HT\*LX/MA\*(JMEGA+MM1\*NBLADE)  
TERM1=PHIXHT(PHIARG)\*(ABS(FHAT(FARG)))\*\*2  
DO 6023 MW1=-MW1MAX,MW1MAX  
THEARG=((MW1\*NVANE)-(MM1\*NBLADE)-MM)\*LTHETA/R  
TURM1=TERY1\*PHITHH(THEARG)  
SUMTUT(MINDEX,IRNU)=SUMTUT(MINDEX,IRNU)+TURM1  
6000 CONTINUE  
WRITE(21,6015) MM,OMEGA,R,SUMTOT(MINDEX,IRNU)  
6015 FORMAT(" M=" ,15," OMEGA=" ,E10.4," R=" ,E10.4," SUMTOT=" ,E10.4)  
C  
C  
6020 CONTINUE  
ISUMTO(MINDEX)=1

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C  
C 6040 CONTINUE  
C  
C ORIGINAL PAGE IS  
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C  
C  $\text{BETASQ} = 1. - \text{MA}^{**2}$   
C  $\text{KMNS} = (((\text{OMEGA}^*\text{MT})^{**2} - 3\text{BETASQ}^*\text{XMN}^{**2})^{**.5}) * \text{ABS}(\text{OMEGA})/\text{OMEGA}$   
C WRITE(21,7018) KMNS  
C 7018 FORMAT(" KMNS=",310.4)  
C  
C CHECK TO BE SURE MODE NUMBER M IS IN RANGE OF STORED DATA  
C  
C IF(MM.LT.0) GO TO 300  
C  
C FOR POSITIVE M, WANT 0.LE.M.LE.(NVANE-1)  
C  
C IF(0.LE.MM.AND.MM.LE.(NVANE-1)) GO TO 310  
C  
C IF M POSITIVE BUT OUT OF RANGE, SUBTRACT INTEGER\*NVANE  
C  
C MTRIAL = MM  
C NTRIAL=0  
C 320 CONTINUE  
C NTRIAL=NTRIAL+1  
C MSUM=MTRIAL-NTRIAL\*NVANE  
C IF(0.LE.MSUM.AND.MSUM.LE.(NVANE-1)) GO TO 330  
C GO TO 320  
C MUSE=MSUM+1  
C GO TO 340  
C  
C FOR NEGATIVE M, ADD INTEGER\*NVANE TO M  
C  
C 300 MTRIAL=MM  
C NTRIAL=0  
C 350 CONTINUE  
C NTRIAL=NTRIAL+1  
C MSUM=MTRIAL+NTRIAL\*NVANE  
C IF(0.LE.MSUM.AND.MSUM.LE.(NVANE-1)) GO TO 360  
C GO TO 350  
C 360 MUSE=MSUM+1  
C GO TO 340  
C  
C 310 MUSE=MM+1  
C  
C 340 CONTINUE  
C  
C 341 FORMAT(" MM=",I5," MUSE=",I5)  
C  
C KILL PROGRAM IF DESIRED FREQUENCY IS OUT OF RANGE  
C OR STORED DATA

C  
C  
PSTART=FLOAT(PSTART)  
PENDF=FLOAT(PEND)  
IF(PSTARTF.LE.OMEGA.AND.3MEGA.LE.PENDF) GO TO 343  
WRITE(5,342)

342 FORMAT(' FREQUENCY OUT OF RANGE OF DATA')  
STOP

343 CONTINUE

C  
C  
SEARCH HARMONIC ORDERKS FOR FREQUENCY INTERPOLATION  
C  
C  
WANT PMIN.LE.OMEGA.LE.PMAX  
C

NUPMIN=PSTART

NUPMAX=PEND  
DO 10 P=PSTART,PEND-PSTEP,PSTEP

IF (UMEGA.GE.(1.\*P)) NUPMIN=P

10 CONTINUE

DO 20 P=PEND,PSTART,-PSTEP

IF (OMEGA.LT.(1.\*P)) NUPMAX=P

20 CONTINUE

C  
C  
C  
C  
C  
CONVERT TO FIND IP PARAMETER OF DATA STORAGE IN CASCET  
C

IP=0  
DO 25 P=PSTART,PEND,PSTEP

IP=IP+1

IPP=P

IF (NUPMIN.EQ.IPP) IPMIN=IP

IF (NUPMAX.EQ.IPP) IPMAX=IP

25 CONTINUE

C  
21 FORMAT(" NUPMIN=",I5," NUPMAX=",I5)  
22 FORMAT(" IPMIN=",I5," IPMAX=",I5)

C  
C  
C  
110 XSIGN=1.

C\*\*\*\*\* RETURN TO LINE (111) TO REPEAT FOR DOWNSTREAM  
C PROPAGATION \*\*\*\*\*

111 GMNS=(NT\*NA\*OMEGA+XSIGN\*K4NS)/BETASQ

C  
C  
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C <MTHEOBALD>@ATURH.FOR;1@ Fri 12-Dec-80 2:09PM PAGE 1:5

C INITIALIZE VARIABLES  
C ISUMR IS ERROR CODE ACCUMULATOR FOR BESSSEL WEIGHTING FUNCTION  
C \*\*S  
C  
C PMNS IS RESULT OF DOUBLE INTEGRAL  
C  
C S\*TR IS WEIGHTING SIGN FUNCTION IN RADIAL INTEGRATION  
C  
C PMNS=0.  
C DELTAR=(1.-SIGMAR)/(NRADNJ-1)  
C ISUMR=0  
C IDOT=2  
C IDAT=2  
C  
C S\*TR=-1.  
C C\*\*\*\*\*START RADIAL INTEGRATION LOOP HERE \*\*\*\*\*  
C  
C DO 901 IRNU=1,NRADNU  
C  
C  
C RADIAL POSITION SEARCH FOR INTERPOLATION COORDINATES  
C  
C WANT RR(IRMIN).LE.RRNU(IRNU).LE.RR(IRMAX)  
C \*\*\*NOTE: RR(1)=RRNU(1)  
C RR(NRAD)=RRNU(NRADNU)  
C  
C IF (IRNU.EQ.1) GO TO 50  
C IF (IRNU.EQ.NRADNU) GO TO 60  
C IRMIN=1  
C IRMAX=NRAD  
C DO 30 IR=1,NRAD-1,1  
C IF (RRNU(IRNU).GE.RR(IR)) IRMIN=IR  
30 CONTINUE  
C DO 40 IR=NRAD,1,-1  
C IF (RRNU(IRNU).LE.RR(IR)) IRMAX=IR  
40 CONTINUE  
C GO TO 70  
50 CONTINUE  
C IRMIN=1  
C IRMAX=2  
C GO TO 70  
60 CONTINUE  
C IRMIN=NRAD-1  
C IRMAX=NRAD  
C GO TO 70  
70 CONTINUE

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```

71      FORMAT(" IRMIN=",I5," IRMAX=",I5)
72      FORMAT(" RR(IRMIN=",E10.4," RRNU(NU=",E10.4," RR(IRMAX=",E10.4)
C
C
C     BLADE GEOMETRY AT RADIAL STATION OF INTEGRATION
      R=RRNU(IRNU)
      IF(R.LE.VGEOM(IDAT,1)) GO TO 201
      IDAT=IDAT+1
      IF(IDAT.GT.NDAT) IDAT=NDAT
201      DELTA=(R-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
      DO 210 IX=2,3
210      XX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))
C
C
      B=XX(1)/2.
      THETA=XX(2)
      WRITE(21,7010) B,THETA,R
7010      FORMAT(" B=",E10.4," THETA=",E10.4," R=",E10.4)
C
C
C
      COSTHE=COS(THETA)
      SINTHE=SIN(THETA)

C
C
      IF (IVOR.EQ.0) GO TO 4020

C
C
C     INTERPULATE TO GET MEAN CIRCUMFERENTIAL MACH NUMBERS AT THIS R
C
C
      IF (R.LE.VELOCV(IDOT,1)) GO TO 4001
      IDOT=IDOT+1
      IF (IDOT.GT.NVELO) IDOT=NVELO
4001      DELTA=(R-VELOCV(IDOT,1))/(VELOCV(IDOT,1)-VELOCV(IDOT-1,1))
      XVEL=VELOCV(IDOT,2)+DELTA*(VELOCV(IDOT,2)-VELOCV(IDOT-1,2))
      MTHETA=XVEL*MA
C
      4015      FORMAT(" R=",E10.4," MTHETA=",E10.4)
C
      4020      CONTINUE

C
C
      MYM IS CIRCUMFERENTIAL MACH NUMBER OF WAKS IMPINGING ON STATOR
C
      MYM=MT*R-MA*MUV/R
      IF (IVOR.EQ.1, MYM=MT*R-MTHETA)
      IF (IVOK.EQ.0) MTHETA=MA*MUV/R

```

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C <MTHEUBALD>=ATURB.FUR;10 Fri 12-Dec-80 2:09PM PAGE 1:7

C CHI IS ARCTAN(CIRCUMFERENTIAL VELOCITY OF WAKE/AXIAL VELOCITY)  
C CHI=ATAN2(MYM,MA)  
C COSCHI=COS(CHI)

C  
C ZMOD=SIGMAC\*B\*(GMNS\*COSTHE-MM\*SINTHE/R)

C CHORDWISE INTEGRATION USES BESSEL INTEGRATION METHOD

C ---CALCULATE BESSEL WEIGHTING FUNCTIONS

C BESJ REQUIRES POSITIVE ARGUMENT

X=ABS(ZMOD)

CALL BESJ(X,B,BJ0,EB,IRROR1)

CALL BESJ(X,NCHORD,BJ(NCHORD),EB,IRROR2)

CALL BESJ(X,NCHORD-1,BJ(NCHORD-1),EB,IRROR3)

ISERR=IRROR1+IRROR2+IRROR3

5400 FORMAT("ZMOD=",E10.4,"ISERR=",I5)

IF(ZMOD.GT.0.) GO TO 5400

C BJ0 IS EVEN FUNCTION, ADJUST SIGN ON OTHERS

BJ(NCHORD)=BJ(NCHORD)\*(-1.)\*\*NCHORD

BJ(NCHORD-1)=BJ(NCHORD-1)\*(-1.)\*\*(NCHORD-1)

5400 CONTINUE

C USE RECURSION RELATION TO COMPUTE AND STORE BESSEL FUNCTIONS

DO 2080 N=NCHORD-1,2,-1

BJ(N-1)=-BJ(N+1)+2.\*N\*BJ(N)/ZMOD

2080 CONTINUE

C  
C  
C

INITIALIZE INTERPOLATION TO GET PRESSURE VALUE FOR THIS  
FREQUENCY AND RADIAL POSITION FROM STORED DATA

C USE 4 POINT BIVARIATE INTERPOLATION. SEE ABRAMOWITZ AND  
C STEGUN 25.2.65

C NOTE QQ AND PP ARE LESS THAN 1

C DETERMINE FRACTIONAL PARTS OF FREQ. AND RADIAL SPACING

PP=(RRNU(IRNU)-RR(IRMIN))/(RR(IRMAX)-RR(IRMIN))

QQ=(OMEGA-NUPMIN)/(NUPMAX-NUPMIN)

C  
C 912 FORMAT(" PP=",E10.4," QQ=",E10.4)

C  
C 4MNS=(0.,0.)

C \*\*\*\*\* BEGIN CHORDWISE INTEGRATION LOOP HERE \*\*\*\*\*

C DO 220 IZ=1,NCHORD ORIGINAL PAGE IS  
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C  
C COMPUTE R SUB S, THE WEIGHTING FUNCTION AT THE CHORDAL  
C STATION  
C NOTE THAT Z=I\*\*IKOUNT BELOW.

C  
RRRS=(0.,0.)  
Z=(1.,0.)  
DO 5000 IKOUNT=0,NCHORD  
BN=1.  
IF(IKOUNT.EQ.0.OR.IKOUNT.EQ.NCHORD) BN=0.5  
ARGU=IKOUNT\*I\*PI/NCHORD  
IF(IKOUNT.GT.0) GO TO 5010  
RRS=BN\*Z\*BJS  
GO TO 5020  
5010 CONTINUE  
RRS=BN\*Z\*BJS(IKOUNT)\*COS(ARGU)  
5020 CONTINUE  
Z=Z\*I  
RRRS=RRRS+RRS  
5000 CONTINUE  
C  
RRRS=RRRS\*2.\*PI/NCHORD  
BN=1.  
IF(I\*EQ.NCHORD) BN=0.5

C  
C INTERPOLATE PRESSURE VALUES IN FREQUENCY AND RADIUS  
C

MCOUNT=MUSE  
Y=(1.-PP)\*(1.-QQ)\*CASSET(I\*,IRMIN,MCOUNT,IPMIN)  
Y=Y+PP\*(1.-QQ)\*CASSET(I\*,IRMAX,MCOUNT,IPMIN)  
Y=Y+QQ\*(1.-PP)\*CASSET(I\*,IRMIN,MCOUNT,IPMAX)  
Y=Y+PP\*QQ\*CASSET(I\*,IRMAX,MCOUNT,IPMAX)

C  
2 FORMAT(" CASSET=",2E10.4)

C  
C EVALUATE FINITE CHORDWISE SUM TO APPROX. INTEGRAL  
C

QMNST=Y\*RRRS\*BN  
QMNS=QMNS+Y\*RRRS\*BN

5030 FORMAT(" I\*=",I5," QMNST=",2E10.4)  
220 CONTINUE

C\*\*\*\*\*END OF CHORDWISE INTEGRATION LOOP (220) \*\*\*\*\*

7022 FORMAT(" IRNU=",I3," QMNS=",2E10.4)

C  
C  
1SUMR=1SUMR+1SER  
7021 CONTINUE

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C <MTHEOBALD>@TURB.FOR;10 Fri 12-Dec-80 2:09PM PAGE 1:9

C  
C

CA=MM\*COSTHE/R+GMNS\*SINTH  
CB=(CA\*BS(GMNS)\*PSISTU(IRNU)\*CA\*8)\*\*2  
CD=((MT\*R)\*\*2+1.)\*\*.5

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C  
C  
C  
C  
C  
C

FMNS=CB\*CD\*SUNTJ1(MINDEX,IRNU)/(R\*\*2)/COSCHI

C  
C

WHTR=1.+SWTR/3.  
SWTR=-SWTR  
IF(IR.EQ.1.OR.IR.EQ.NRAD) WHTR=WHTR/2.

C  
C

7016 PMNS=PMNS+WHTR\*FMNS\*DELTAR/R  
FORMAT('PMNS SUM(R)=',E10.4)  
901 CONTINUE

C

C\*\*\*\*\* END OF RADIAL INTEGRATION LOOP (901) \*\*\*\*\*

C

CC=LR\*LTHETA\*LX\*(EPSW\*WWIDTH)\*\*2

C  
C

SMN=((BETASQ\*NBLADE\*NVANE)\*\*2)\*MT\*OMEGA\*PMNS/KMNS\*MA\*\*3  
SMN=SMN/(1.-SIGMAR\*\*2)/(OMEGA\*MT\*XSGV\*MA\*KMNS)\*\*2  
SMN=SMN\*CC\*SIGMAC\*SIGMAC\*(-XSIGN)/32./(PI\*\*4)

C

C

MULTIPLY OUTPUT BY 2 (ADDS +3DB) TO ACCOUNT FOR ENERGY  
IN NEGATIVE FREQUENCY  
SMN=SMN\*2.

C

RELPW=R=SMN  
IPWR=1  
IF(RELPWR.EQ.0.) GO TO 915  
RELPRL=10.\*ALJG10(ABS(RELPWR))  
GU TU 920

915

IPWR=0

920

CONTINUE

C

CC

C

IF(XSIGN.LT.0.) GJ TO 9000

C

WRITE(5,3000)

```
3000 FORMAT("UPSTREAM")
8101 FORMAT(" GAMMA M,N,SB =",E16.8)
WRITE(21,8102) SMN
8102 FORMAT(" REL. MODAL SOUND POWER SPECTRAL DENSITY=",E16.4)
WRITE(21,8500) IER
WRITE(21,5500) ISUMR
8500 FORMAT(" SUM OF ALL ERRORS IN PSI CALCULATIONS =",I5)
IF(IPWR.EQ.0) GO TO 970
WRITE(5,8600) RELPRL
GO TO 980
970 CONTINUE
WRITE(5,952)
980 CONTINUE
8600 FORMAT(" REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=",E16.4)
WRITE(21,7200)
7200 FORMAT("END OF UPSTREAM INTEGRATION")
XSIGN=-1.
SPWR(1)=RELPWR
GO TO 111
```

C  
\*\*\*\*\* RETURN TO LINE 111 TO COMPUTE DOWNSTREAM PROPAGATION  
\*\*\*\*\*

```
C
9000 WRITE(5,8200)
8200 FORMAT("DOWNSTREAM")
8201 FORMAT(" GAMMA M,N,SB =",E16.8)
WRITE(21,8202) SMN
8202 FORMAT(" REL. MODAL SOUND POWER SPECTRAL DENSITY=",E16.4)
WRITE(21,8400) IER
WRITE(21,5500) ISUMR
5500 FORMAT(" SUM OF ALL ERRORS IN RS CALCULATIONS =",I5)
8400 FORMAT(" SUM OF ALL ERRORS IN PSI CALCULATIONS =",I5)
IF(IPWR.EQ.0) GO TO 950
WRITE(5,8600) RELPRL
GO TO 960
950 CONTINUE
WRITE(5,952)
952 FORMAT(" SOUND POWER SPECTRAL DENSITY FOR MODE=0/UNEXCITED")
960 CONTINUE
SPWR(2)=RELPWR
WRITE(21,7202)
7202 FORMAT("END OF DOWNSTREAM INTEGRATION")
RETURN
END
```

## SUBROUTINE ANRT

Program finds the roots of the boundary value equation for an annular duct.

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C  
C  
C .....

SUBROUTINE ANRT(M,N,S,EB,EC,XMN,IEB,IEC)

(AN)NULAR FUNCTION (R)0J(T)

PURPOSE  
START WITH A GUESS SOLUTION FOR XM1  
AND GET A BETTER VALUE FOR XM1.  
GUESS EACH HIGHER ORDER ROOT FROM  
 $XM(N+1) = XMN + 3.14159$   
AND THEN REFINE IT TO GET THE (M,N)  
ROOT TO :  $F=P(JS^*Y-YS^*J) = 0$

.....

IF(M.EQ.0.AND.N.EQ.1) GO TO 6  
XMN = M-3.14159  
DO 5 NN=1,N  
DX = .31415  
IS = (-1)\*\*(NN+1)  
X = XMN+3.14159  
J = 1

C  
CALL ANFU(M,X,S,EB,F,IEB)  
DX = -ISIG(F\*IS)\*DX  
TE = F

C 1 IF (ABS(F) .LE. EC) GO TO 3  
IF (J .GT. 100) GO TO 2

C  
X = X+DX  
CALL ANFJ(M,X,S,EB,F,IEB)

C  
IF ((F\*TE) .LT. 0.) DX = -DX/2.  
J = J+1  
TE = F  
GO TO 1

C 2 IEC = 1  
GO TO 4

C 3 IEC = 0

C 4 XMN = X

C 5 CONTINUE

6 RETURN  
CONTINUE  
IEB=0  
IEC=0  
XMN=0.  
RETURN  
END

~L

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C <MTHEOBALD>ANRT.FOR;3 Mon 14-Jan-80 6:31PM

PAGE 2

C  
C .....  
C  
SUBROUTINE ANFU(M,X,S,EB,F,IEB)  
C  
(AN)NULAR (P)UNCTION  
C  
PURPOSE  
EVALUATE THE DETERMINANT F = P(JS\*Y-ZY\*S)  
C  
.....  
C  
IF (M .NE. 0) GO TO 1  
CALL BESJ( X,1,ZJ ,EB ,IE3)  
CALL BESJ(S\*X,1,ZJS ,EB ,IE4)  
CALL BESY( X,1,ZY , IE7)  
CALL BESY(S\*X,1,ZYS , IE8)  
IEB = IE3+IE4+IE7+IE8  
GO TO 2  
C  
1 CALL BESJ( X,M-1,BJM ,EB ,IE1)  
CALL BESJ(S\*X,M-1,BJMS,EB ,IE2)  
CALL BESJ( X,M+1,BJP ,EB ,IE3)  
CALL BESJ(S\*X,M+1,BJPS,EB ,IE4)  
ZJ = .5\*(BJM -BJP )  
ZJS = .5\*(BJMS-BJPS)  
CALL BESY( X,M-1,BYM , IE5)  
CALL BESY(S\*X,M-1,BYMS, IE6)  
CALL BESY( X,M+1,BYP , IE7)  
CALL BESY(S\*X,M+1,BYPS, IE8)  
ZY = .5\*(BYM -BYP )  
ZYS = .5\*(BYMS-BYPS)  
IEB = IE1+IE2+IE3+IE4+IE5+IE6+IE7+IE8  
C  
2 F = ZJS\*ZY - ZJ\*ZYS  
RETURN  
END

SUBROUTINE BESJ

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PURPOSE

COMPUTE THE J BESSSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER

USAGE

CALL BESJ(X,N,BJ,D,IER)

DESCRIPTION OF PARAMETERS

X -THE ARGUMENT OF THE J BESSSEL FUNCTION DESIRED

N -THE ORDER OF THE J BESSSEL FUNCTION DESIRED

BJ -THE RESULTANT J BESSSEL FUNCTION

D -REQUIRED ACCURACY

IER-RESULTANT ERROR CODE WHERE

IER=0 NO ERROR

IER=1 N IS NEGATIVE

IER=2 X IS NEGATIVE OR ZERO

IER=3 REQUIRED ACCURACY NOT OBTAINED

IER=4 RANGE OF N COMPARED TO X NOT CORRECT (SEE REMARKS)

REMARKS

N MUST BE GREATER THAN OR EQUAL TO ZERO, BUT IT MUST BE  
LESS THAN

$20 \times 10^6$  FOR X LESS THAN OR EQUAL TO 15

$90 \times 10^6$  FOR X GREATER THAN 15

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

NONE

METHOD

RECURRENCE RELATION TECHNIQUE DESCRIBED BY H. GOLDSTEIN AND  
R.M. THALER, "RECURRENCE TECHNIQUES FOR THE CALCULATION OF  
BESSEL FUNCTIONS", M.T.A.C., V.13, PP.102-108 AND I.A. STEGUN  
AND M. ABRAMOWITZ, "GENERATION OF BESSEL FUNCTIONS ON HIGH  
SPEED COMPUTERS", M.T.A.C., V.11, 1957, PP.255-257

SUBROUTINE BESJ(X,N,BJ,D,IER)

BJ=.0

IF (X .NE. 0.) GO TO 9

IER = 0

IF (N .EQ. 0) BJ = 1.

RETURN

C  
9 IF(N)10,20,20  
10 IER=1  
RETURN  
20 IF(X)30,30,31  
30 IER=2  
RETURN  
31 IF(X-15.)32,32,34  
32 NTEST=20.+10.\*X-X\*\* 2/3  
GO TO 36  
34 NTEST=90.+X/2.  
36 IF(N-NTEST)40,38,38  
38 IER=4  
RETURN  
40 IER=0  
N1=N+1  
BPREV=.0

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C  
C COMPUTE STARTING VALUE OF M  
C  
50 IF(X-5.)50,50,60  
MA=X+6.  
GO TO 70  
60 MA=1.4\*X+60./X  
70 MB=N+IFIX(X)/4+2  
MZERO=MAX0(MA,MB)

C  
C SET UPPER LIMIT OF M  
C

100 MMAX=NTEST  
DO 190 M=MZERO,MMAX,3

C  
C SET F(M),F(M-1)  
C  
FM1=1.0E-28  
FM=.0  
ALPHA=.0  
IF(M-(M/2)\*2)120,110,120  
110 JT=-1  
GO TO 130  
120 JT=1  
M2=M-2  
DO 160 K=1,M2  
MK=M-K  
BMK=2.\*FLOAT(MK)\*FM1/X-FM  
FM=FM1  
FM1=BMK  
IF(MK-N-1)150,140,150  
140 BJ=BMK  
JT=-JT  
S=1+JT

C <MTHEOBALD>ANRT.FOR;3 Mon 14-Jan-80 6:31PM

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```
160 ALPHA=ALPHA+BMK*S
BMK=2.*FM1/X-FM
IF(N)180,170,180
170 BJ=BMK
180 ALPHA=ALPHA+BMK
BJ=BJ/ALPHA
IF(ABS(BJ-BPREV)-ABS(D*BJ))200,200,190
190 BPREV=BJ
IER=3
RETURN
END
```

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C SUBROUTINE BESY  
C

## C PURPOSE

C COMPUTE THE Y BESSSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER

## C USAGE

C CALL BESY(X,N,BY,IER)

## C DESCRIPTION OF PARAMETERS

C X -THE ARGUMENT OF THE Y BESSSEL FUNCTION DESIRED

C N -THE ORDER OF THE Y BESSSEL FUNCTION DESIRED

C BY -THE RESULTANT Y BESSSEL FUNCTION

C IER-RESULTANT ERROR CODE WHERE

C IER=0 NO ERROR

C IER=1 N IS NEGATIVE

C IER=2 X IS NEGATIVE OR ZERO

C IER=3 BY HAS EXCEEDED MAGNITUDE OF 10\*\*70

## C REMARKS

C VERY SMALL VALUES OF X MAY CAUSE THE RANGE OF THE LIBRARY  
C FUNCTION ALGO TO BE EXCEEDED

C X MUST BE GREATER THAN ZERO

C N MUST BE GREATER THAN OR EQUAL TO ZERO

## C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

C NONE

## C METHOD

C RECURRENCE RELATION AND POLYNOMIAL APPROXIMATION TECHNIQUE  
C AS DESCRIBED BY A.J.M. HITCHCUCK, "POLYNOMIAL APPROXIMATIONS  
C TO BESSEL FUNCTIONS OF ORDER ZERO AND ONE AND TO RELATED  
C FUNCTIONS", M.T.A.C., V.11, 1957, PP.36-88, AND G.N. WATSON,  
C "A TREATISE ON THE THEORY OF BESSEL FUNCTIONS", CAMBRIDGE  
C UNIVERSITY PRESS, 1958, P. 62C .....  
C SUBROUTINE BESY(X,N,BY,IER)

C CHECK FOR ERRORS IN N AND X

C IF(N)180,10,10

10 IER=0

IF(X)190,190,20

C BRANCH IF X LESS THAN OR EQUAL 4

20 IF(X-4.0)40,40,30

C  
C COMPUTE Y0 AND Y1 FOR X GREATER THAN 4

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```
30 T1=4.0/X
T2=T1*T1
P0=((((-.0000037043*T2+.0000173565)*T2-.0000487613)*T2
1 +.00017343)*T2-.001753062)*T2+.3989423
Q0=((((.0000032312*T2-.0000142078)*T2+.0200342468)*T2
1 -.0000869791)*T2+.0004564324)*T2-.01246594
P1=((((.0000042414*T2-.0000200920)*T2+.0000580759)*T2
1 -.000223203)*T2+.002921825)*T2+.3989423
Q1=((((-.0000035594*T2+.00001622)*T2-.0000398708)*T2
1 +.0001064741)*T2-.0005390400)*T2+.03740084
A=2.0/SQRT(X)
B=A*T1
C=X-.7853982
Y0=A*P0*SIN(C)+B*Q0*COS(C)
Y1=-A*P1*COS(C)+B*Q1*SIN(C)
GO TO 90
```

C  
C COMPUTE Y0 AND Y1 FOR X LESS THAN OR EQUAL TO 4

```
40 XX=X/2.
X2=XX*XX
T= ALOG(XX)+.5772157
SUM=0.
TERM=T
Y0=T
DO 70 L=1,15
IF(''-1)5^,60,50
50 SUM=SUM+1./FLOAT(L-1)
60 FL=L
TS=T-SUM
TERM=(TERM*(-X2)/FL**2)*(1.-1./(FL*TS))
70 Y0=Y0+TERM
TERM = XX*(T-.5)
SUM=0.
Y1=TERM
DO 80 L=2,16
SUM=SUM+1./FLOAT(L-1)
FL=L
FL1=FL-1.
TS=T-SUM
TERM=(TERM*(-X2)/(FL1*FL))*((TS-.5/FL)/(TS+.5/FL1))
80 Y1=Y1+TERM
PI2=.6366198
Y0=PI2*Y0
Y1=-PI2/X+PI2*Y1
```

C  
C CHECK IF ONLY Y0 OR Y1 IS DESIRED

90 IF(N-1)100,100,130

C  
C RETURN EITHER Y0 OR Y1 AS REQUIRED

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100 IF(N)110,120,110  
110 BY=Y1  
GO TO 170  
120 BY=Y0  
GO TO 170

C  
C PERFORM RECURRENCE OPERATIONS TO FIND YN(X)

130 YA=Y0  
YB=Y1  
K=1  
140 T=FLOAT(2\*K)/X  
YC=T\*YB-YA  
IF(ABS(YC)-1.7E33)145,145,141  
141 IER=3  
RETURN  
145 K=K+1  
IF(K-N)150,160,150  
150 YA=YB  
YB=YC  
GO TO 140  
160 BY=YC  
170 RETURN  
180 IER=1  
RETURN  
190 IER=2  
RETURN  
END

SUBROUTINE CASC

Program computes the complex pressure distribution across a blade chord for incident turbulence.

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(\*)

## SUBROUTINE EIGEN

Program computes the weighting factors for the eigen functions (mode shapes).

PREVIOUS PAGE: SLIDES NOT FOLDED

```
SUBROUTINE EIGEN(MM,STGMAR,XMN,BMN,D,IER)
DIMENSION IER(8)
IF(XMM.EQ.0.) GO TO 22
N=MM
IF(N.LT.0) N=-N
MMINUS=IAPS(N-1)
MPLUS=N+1
XMHUP=XMH*SIGMAR
S=SIGMAR**2
CALL BESJ (XMM,N,BJM,D,IER(1))
CALL BESY (XMM,N,BYM,D,IER(2))
CALL BESJ (XMHUP,N,BJMH,D,IER(3))
CALL BESY (XMHUP,N,BYMH,D,IER(4))
CALL BESJ (XMM,MPLUS,BJMP,D,IER(5))
CALL BESY (XMM,MPLUS,BYMP,D,IER(6))
CALL BESJ (XMM,MMINUS,BJMM,D,IER(7))
CALL BESY (XMM,MMINUS,BYMM,IER(8))
IF(N.GT.0) GO TO 100
BJMV=-BJMV
BYMV=-BYMV
100 BJPRIM=(BJMV-BJMP)/2.
BYPRIM=(BYMV-BYMP)/2.
IF(.ABS(BJPRIM).LT.ABS(BYPRIM)) GO TO 10
AVN=-BYPRIM/BJPRIM
BVN=1.
GO TO 24
10 AVN=1.
BMN=-BJPRIM/BYPRIM
20 PART1=(1.-(MM/XMN)**2)*(AMM*BJM+BMN*BYM)**2/(1.-S)
PART2=(S-(MM/YMM)**2)*(AMM*BJMH+BMN*BYMH)**2/(1.-S)
FACTOR=(PART1-PART2)**.5
AVN=AMN/FACTOR
BMN=BVN/FACTOR
RETURN
22 CONTINUE
AVN=1.
BMN=0.
24 DO 24 J=1,8
IER(J)=0
RETURN
END
```

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SUBROUTINE EPSD

Program yields the inlet RMS  
turbulence intensity.

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### SUBROUTINE FHAT

Program computes the Fourier  
transform of the spatial  
distribution of wake turbulence.

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## FUNCTION FHAT(FARG)

C  
C FUNCTION YIELDS THE FOURIER TRANSFORM OF THE SPATIAL  
C DISTRIBUTION OF WAKE TURBULENCE VELOCITY FOR  
C SUBROUTINE OUTURB  
C  
C DATA PI/3.14159/  
C  
C NEED SWITCH TO AVOID UNDERFLOW ON EXPONENTIAL :  
C RANGE IS E+38.  
C  
A=(FARG\*\*2)/4./PI  
IF(A.GT.87.) GO TO 10  
B=EXP(-A)  
GO TO 20  
10 S=0.  
20 CONTINUE  
FHAT=B  
RETURN  
END

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## SUBROUTINE KERNEL

Program computes the kernel  
of the Green's function.

```

SUBROUTINE KERNEL(X,K,GAMMA,MR,H1,H2,ERROR,CKF)
REAL K,MR
COMPLEX I,CKF,AN,ANP,ANM,RN,RJOT
RN(AN)=BETAR**2*H2/(2.*D**2)*(AN**2-K**2)*CEXP(I*(AN+K*MR))
1 *X)/((AN-GN*H1/D**2)*(AN+K/MR))
DATA I/(0.,1.)/,PI/3.14159/,XMIN/.001/
BETAR=SQRT(1.-MR**2)
IF(ABS(X).GT.XMIN) GO TO 10
CKF=BETAR/(2.*PI)*CEXP(-I*BETAR**2*K*X/MR)*(1./X-I*K/MR
1 * ALOG(ABS(X)))
RETURN
10 CONTINUE
D=SQRT(H1**2+(BETAR**2)**2)
R=D*SQRT(K**2+(D*ALOG(ERROR)/(BETAR**2*X))**2)
N1=(GAMMA-R)/(2.*PI)
N2=(GAMMA+R)/(2.*PI)
CKF=0.
IF(X.GT.0.) G1 TO 50
DO 40 N=N1,N2
GN=GAMMA-2.*PI*N
S=(K*D)**2-GN**2
IF(S.GE.0.) RJOT=-SQRT(S)*ABS(K)/K
IF(S.LT.0.) RJOT=I*SQRT(-S)
ANM=(GN*H1-BETAR**2*RJOT)/D**2
CKF=CKF+RN(ANM)
40 CONTINUE
RETURN
50 CONTINUE
DO 70 N=N1,N2
GN=GAMMA-2.*PI*N
S=(K*D)**2-GN**2
IF(S.GE.0.) RJOT=-SQRT(S)*ABS(K)/K
IF(S.LT.0.) RJOT=I*SQRT(-S)
ANP=(GN*H1+BETAR**2*RJOT)/D**2
CKF=CKF-RN(ANP)
70 CONTINUE
CKF=CKF-BETAR**2*K/(2.*MR)*SINH(BETAR**2*K
1 *H2/MR)*CEXP(-I*BETAR**2*K*X/MR)/(COSH(BETAR**2*K*X/MR)-
2 COS(GAMMA+K*H1/MR))
RETURN
END

```

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## SUBROUTINE PHITHH

Program computes the Fourier transform of the correlation function in the circumferential direction.

C <MTHEOPALD>PHITHH.FOR;3 Tue 22-Jan-80 3:27PM PAGE 1

FUNCTION PHITHH(ARGUM2)

C  
C  
C PROGRAM CALCULATES THE FOURIER TRANSFORM OF THE CORRELATION  
C FUNCTION IN THE AZIMUTHAL DIRECTION AS A FUNCTION OF  
C  
C  
C 12/14/79 VERSION USES GAUSSIAN AUTOCORRELATION FUNCTION.  
C FORM FOLLOWS EQUATION 27 IN W.D. MARK'S "ROTOR INLET  
C TURBULENCE" PAGE 10.

C DATA PI/3.14159/

C  
C NEED SWITCH TO AVOID UNDERFLOW IN EXPONENTIATION. RANGE  
C IS E+-38.

C  
A=ARGUM2\*\*2  
B=A/PI  
IF(B.GT.87.) GO TO 10  
C=2.\*EXP(-B)  
GO TO 20  
10 C=0.  
20 CONTINUE  
PHITHH=C  
RETURN  
END

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## SUBROUTINE PHIXHT

Program calculates the Fourier transform of the correlation function in the axial direction.

C <MTHEODAL>PHIXHT.FOR;3 Tue 22-Jan-87 3:19PM PAGE 1

FUNCTION PHIXHT(ARGUM1)

C  
C PROGRAM CALCULATES THE FOURIER TRANSFORM OF THE CORRELATION  
C FUNCTION IN THE AXIAL DIRECTION AS A FUNCTION OF  
C NONDIMENSIONAL FREQUENCY

C  
C  
C 12/14/79 VERSION USES GAUSSIAN AUTOCORRELATION FUNCTION.  
C FORM FOLLOWS EQUATION 27 IN W.D. MARK'S "ROTOR INLET  
C TURBULENCE" PAGE 18.

C  
C  
C NEED SWITCH TO AVOID UNDERFLOW ON EXPONENTIATION. RANGE  
C IS E+38

C  
DATA PI/3.14159/  
A=ARGUM1\*\*2  
B=A/PI  
IF(B.GT.87.) GO TO 10  
C=2.\*EXP(-B)  
GO TO 20  
10 C=0.  
20 CONTINUE  
PHIXHT=C  
RETURN  
END

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## SUBROUTINE PRES

Program generates the complex pressure distribution across the stator vane chord.

```

SUBROUTINE PRES(WH,VX,K,GAMMA,MR,H1,H2,MSEG,F,IER)
REAL K,VR,KX
COMPLEX I,WH,F,A,CKF
COMPLEX G,G0,G1,G2,G3
DIMENSION F(100),I(100,100),A(100),B(100)
DATA I/(0.,1.)/,ERR0R/.0001/,PI/3.14159/
DATA (B(J),J=1,100)/100*1.0/
G(X)=(G0+G1*X+G2*X**2+G3*X**3)*CEXP(I*K*MR*X)
B(MSEG)=.5
BETAR=SQRT(1.-MR**2)
G0=I*BETAR*K/(2.*PI*MR)
G1=BETAR*K**2/(2.*PI)*(1./MR**2-0.5)
G2=I*BETAR*K**3/(4.*PI)*(1./(2.*MR)-1./VR**3)
G3=-BETAR*K**4/(12.*PI)*(1./MR**4-1./(2.*VR**2)-2.125)
DO 10 M=1,MSEG
X=COS((V-.5)*PI/MSEG)
F(M)=WH*CEXP(I*KX*X)
10 CONTINUE
N=MSEG
DO 50 M=1,N
DO 50 L=1,N
S=-ALOG(2.)
DO 40 IR=1,N
S=S-2.*B(IR)/IR*COS((V-.5)*IR*PI/N)*COS(PI*IR*L/N)
40 CONTINUE
ARG=COS((V-.5)*PI/N)-COS(L*PI/N)
CALL KERNEL(ARG,K,GAMMA,MR,H1,H2,ERROR,CKF)
A(M,L)=B(L)*(CKF+G(ARG)*(S-ALOG(ABS(ARG))))*PI/N
50 CONTINUE
CALL LEQTIC(A,MSEG,100,F,1,100,0,WA,IER)
RETURN
END

```

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## SUBROUTINE RMODE

Program computes the radial mode shape for an annular duct.

C <MTHEOBALD>RMODE.FOR;2 Mon 14-Jan-80 12:19PM PAGE 1

Burroughs  
Corporation

```
SUBROUTINE RMODE (M4,X,AMN,BMN,PSI,D,IERROR)
DIMENSION IERROR(2)
IF(X.EQ.0.) GO TO 300
FACTOR=1.
M=MM
IF(M.LT.0) GO TO 100
CONTINUE
CALL BESJ (X,"BJ,D,IERROR(1))
CALL BESY (X,M,BY,IERROR(2))
PSI=FACTOR*(AMN*BJ+BMN*BY)
RETURN
100 M=-M
K=M/2
IF((1.*M)/(2.).GT.(1.*K)) FACTOR=-1.
GO TO 200
200 CONTINUE
PSI=AMN
IERROR(1)=0
IERROR(2)=0
RETURN
END
```

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## SUBROUTINE SCALLR

Program yields the turbulence length scale in the radial direction.

C <MTHEORALD>SCALLR.FOR;6 Mon 29-Sep-80 11:11PM PAGE 1

FUNCTION SCALLP(R)

C  
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH  
C SCALE IN THE RADIAL DIRECTION AS A FUNCTION OF THE MEAN RADIUS.  
C THE LENGTH SCALE IS nondimensionalized ON THE DUCT RADIUS.  
C NOTE SIGVAR.LE.R.LE.1.  
C  
C 12/21/79 VERSION USES A CONSTANT

C  
B=0.50  
SCALLR=B  
RETURN  
END

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## SUBROUTINE SCALLX

Program yields the turbulence  
length scale in the axial  
direction.

C <MTHEOPALD>SCALLY.FOR;4 Mon 29-Sep-83 11:11PM PAGE 1

FUNCTION SCALLY(R)

C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH SCALE  
C IN THE AXIAL DIRECTION AS A FUNCTION OF THE MEAN RADIUS.  
C LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.

C 12/18/79 VEPSTON USES A CONSTANT  
C NOTE SIGMAR.LE.R.LE.1.

R=40.  
SCALLX=8  
RETURN  
END

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## SUBROUTINE STHETA

Program yields the turbulence length scale in the circumferential direction.

C <MTHEODALD>STHETA.FOR;4 Mon 29-Sep-80 11:12PM PAGE 1

FUNCTION STHETA(R)

C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH SCALE  
C IN THE AZIMUTHAL DIRECTION AS A FUNCTION OF MEAN RADIUS.  
C THE LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.

C DATA PI/3.14159/

C 12/18/79 VESTON USES A CONSTANT  
C NOTE SIGMAR.LF.R.LF.1.

B=0.5

STHETA=B

RETURN

END

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**PROGRAM MAPIN/  
SUBROUTINE MAPPER  
(with sample execution)**

Program lists which duct modes  
will propagate for inlet turbu-  
lence noise.

C  
C  
DIMENSION RDATA(20)  
REAL MT,MA

C  
C  
C INPUT VARIABLES TO SUBROUTINE MAPPER FOR LISTING OF ALL  
C PROPAGATING MODES FOR TURBULENCE PROGRAMS AT A  
C GIVEN FREQUENCY

C  
1001 FORMAT(G20.8)  
WRITE(5,2003)  
2003 FORMAT(" HUB RADIUS DIVIDED BY DUCT RADIUS =")  
READ(5,1001) SIGMAR  
WRITE(5,2103) SIGMAR  
2103 FORMAT(" SIGMAR=",E16.8)  
C  
C  
2030 WRITE(5,2030)  
FORMAT(" MT =")  
READ(5,1001) MT  
WRITE(5,2130) MT  
2130 FORMAT(" MT=",E16.8)  
WRITE(5,2031)  
2031 FORMAT(" MA =")  
READ(5,1001) MA  
WRITE(5,2131) MA  
2131 FORMAT(" MA =",E16.8)  
WRITE(5,2037)  
2037 FORMAT(" ACCURACY OF BESSEL FN =")  
READ(5,1001) EB  
WRITE(5,2137) EB  
2137 FORMAT(" EB=",E16.8)  
WRITE(5,2038)  
2038 FORMAT(" ACCURACY OF CONVERGENCE TO ROOT XMN =")  
READ(5,1001) EC  
WRITE(5,2138) EC  
2138 FORMAT(" EC=",E16.8)

C  
C  
C  
C  
RDATA(1)=MT  
RDATA(2)=MA  
RDATA(9)=EB  
RDATA(10)=EC

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C  
C  
RDATA(5)=SIGMAR

C  
CALL MAPPER(RDATA)  
STOP  
END

SUBROUTINE MAPPER(RDATA)  
DIMENSION IER(8),RDATA(20)  
REAL MT, MA

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PROGRAM LISTS ALL PROPAGATING MODES FOR INLET AND WAKE  
TURBULENCE PROGRAMS WITHOUT CALCULATING MODAL  
AMPLITUDES. USE THIS PROGRAM AS A PRECURSOR TO  
INTURB OR WATURB SEARCH ROUTINES TO ESTIMATE RUN TIME.

```
1001 FORMAT(G20.8)
      WRITE(5,110)
110   FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')
      READ(5,1001) OMEGA
      RDATA(8)=OMEGA
115   FORMAT(' OMEGA=',E10.4)
      WRITE(5,115) RDATA(8)
      MT=RDATA(1)
      MA=RDATA(2)
      SIGMAR=RDATA(5)
      EB=RDATA(9)
      EC=RDATA(10)
```

XMAX=OMEGA\*MT/(1.-MA\*\*2)\*\*.5

```
2001 WRITE(5,2001) XMAX
      FORMAT(' XMN(MAX) FOR PROPAGATION =',E16.8)
```

START WITH PLANE WAVE MODE (0,1). COUNT UP IN N, THEN M  
UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

J=1
M=0

RESTART N COUNT HERE FOR NEW M

15 N=0

C <THEOBALD>MAPPER.FOR;3 Fri 29-Feb-80 10:26AM PAGE 1:1

C INCREMENT N  
C  
20 N=N+1 ORIGINAL PAGE IS  
C OF POOR QUALITY  
C  
C MABS=1ABS(M)  
C  
C  
C CALL ANRT (MABS,N,SIGMAR,EB,EC,XMN,IEB,IEC)  
C  
C  
C IF MODE IS CUT OFF, GO TO 6000  
C  
C IF(XMN.GE.XMAX) GO TO 6000  
C  
C  
C WRITE(5,3000)  
3000 FORMAT("MODE DATA")  
WRITE(5,3001) OMEGA,M,N,XMN  
3001 FORMAT("OMEGA=",E10.4," M=",I3," N=",I3," XMN=",E10.4)  
IF(XMN.EQ.0.) GO TO 1000  
COFFRA=XMAX/XMN  
WRITE(5,4000) COFFRA  
4000 FORMAT(" CUTOFF RATIO FOR MODE=",E10.4)  
GO TO 1005  
1000 CONTINUE  
WRITE(5,4005)  
4005 FORMAT(" PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE")  
1005 CONTINUE  
WRITE(5,3002) IEB  
3002 FORMAT(" SUM OF BESSSEL FUNCTION ERROR CODES =",I3)  
WRITE(5,3003) IEC  
3003 FORMAT(" ERROR CODE FOR CONVERGENCE TO ROOT XMN =",I3)  
C  
C NORMALIZE MODE AMPLITUDE  
C  
C CALL EIGN (MABS,SIGMAR,XMN,AMN,BMN,EB,IER)  
C  
C  
C WRITE(5,3004) AMN,BMN  
3004 FORMAT(" AMN =",E16.8," BMN =",E16.8)  
WRITE(5,3005) IER  
3005 FORMAT(" ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC =",8I2)  
C  
C  
C  
C

C  
C  
C        MMM=M    ORIGINAL PAGE IS  
C        DO NOT SWITCH SIGN ON M IF M=0    OF POOR QUALITY  
C        IF(M.EQ.0) GO TO 20  
C  
C        MMM=-MMM  
C  
C        WRITE(5,8300) MMM,N,RDATA(8)  
8300      FORMAT('JM=',I5,' N=',I5,' OMEGA=',E10.4)  
C        SWITCH SIGN ON M  
C  
C  
C  
C        GO TO 20  
C  
C  
C  
C  
C        IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.  
C  
6000      IF(N.EQ.1) GO TO 7000  
C  
C        NMAX=N-1  
C        WRITE(5,6301) NMAX  
6001      FORMAT('LARGEST PROPAGATING N FOR THIS M =',I3)  
C  
C        J=J+1  
C        INCREMENT M  
C  
C        M=M+1  
C        GO TO 15  
C  
C  
C        N=1 TO REACH THIS POINT  
7000      CONTINUE  
C  
C        WRITE(5,7001)  
7001      FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')  
10        CONTINUE  
C        WRITE(5,9001)  
9001      FORMAT(' PROBLEM COMPLETED')  
RETURN  
END

Sample Execution of MAPIN/MAPPER

```
@MAPPER
HUB RADIUS DIVIDED BY DUCT RADIUS =
.484
SIGMAR= 0.48400000E+00
MT =
.508
MT= 0.50800000E+00
MA =
.323
MA = 0.32300000E+00
ACCURACY OF BESSSEL FN =
.0001
EB= 0.10000000E-03
ACCURACY OF CONVERGENCE TO ROOT XMN =
.0001
EC= 0.10000000E-03
NOISE FREQUENCY/SHAFT FREQUENCY=
15.
OMEGA=.1500E+02
XMN(MAX) FOR PROPAGATION = 0.80515728E+01
```

MODE DATA

```
OMEGA=.150.E+02 M= 0 N= 1 XMN=.0000E+00
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE
SUM OF BESSSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = 0.10000000E+01 BMN = 0.00000000E+00
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0
```

MODE DATA

```
OMEGA=.1500E+02 M= 0 N= 2 XMN=.6205E+01
CUTOFF RATIO FOR MODE=.1298E+01
SUM OF BESSSEL FUNCTION ERROR CODES = 0
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0
AMN = -0.26166472E+01 BMN = 0.27171760E+01
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0
```

LARGEST PROPAGATING N FOR THIS M = 2  
%FRSAPR Floating underflow PC= 3100

%FRSAPR Floating underflow PC= 3146

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 1 N= 1 XMN= .1371E+01  
CUTOFF RATIO FOR MODE= .5873E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.15152306E+01 BMN = -0.42119467E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 2 N= 2 XMN= .6390E+01  
CUTOFF RATIC FOR MODE= .1260E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.14355938E+01 BMN = 0.32269858E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -1 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

UNEGA= .1500E+02 M= 2 N= 1 XMN= .2708E+01  
CUTOFF RATIO FOR MODE= .2973E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.20525722E+01 BMN = -0.42471320E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 1 OMEGA= .1500E+02

MODE DATA

OMEG.N= .1500E+02 M= 2 N= 2 XMN= .6920E+01  
CUTOFF RATIO FOR MODE= .1164E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36560635E+01 BMN = 0.74837045E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -2 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 3 N= 1 XMN= .3987E+01

CUTOFF RATIO FOR MODE= .2020E+01

SUM OF BESSLE FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.26023450E+01 BMN = -0.32589376E+00

ERROR CODE FOR BESSLE FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 3 N= 2 XMN= .7747E+01

CUTOFF RATIO FOR MODE= .1039E+01

SUM OF BESSLE FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.35705322E+01 BMN = -0.89511162E+00

ERROR CODE FOR BESSLE FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 4 N= 1 XMN= .5200E+01

CUTOFF RATIO FOR MODE= .1549E+01

SUM OF BESSLE FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.31336392E+01 BMN = -0.20930877E+00

ERROR CODE FOR BESSLE FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -4 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1

C-3

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 5 N= 1 XMN= .6355E+01  
CUTOFF RATIO FOR MODE= .1267E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36182370E+01 BMN = -0.11930907E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .1500E+02 M= 6 N= 1 XMN= .7473E+01  
CUTOFF RATIO FOR MODE= .1077E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.40542452E+01 BMN = -0.61590101E-01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1  
NO MORE PROPAGATING MODES FOR THIS OMEGA  
PROBLEM COMPLETED  
STOP

END OF EXECUTION

CPU TIME: 29.82 ELAPSED TIME: 3:4.03

EXIT.

^C

@MAPPER

HUB RADIUS DIVIDED BY DUCT RADIUS =

.484

SIGMAR= 0.48400000E+00

MT =

.508

MT= 0.50800000E+00

MA =

.323

MA = 0.32300000E+00

ACCURACY OF BESSSEL FN =

.0001

EB= 0.10000000E-03

ORIGINAL PAGE  
OF POOR QUALITY

ACCURACY OF CONVERGENCE TO ROOT XMN =  
.0001  
EC= 0.10000000E-03  
NOISE FREQUENCY/SHAFT FREQUENCY=  
30.  
OMEGA= .3000E+02  
XMN(MAX) FOR PROPAGATION = 0.16103146E+02

MODE DATA

OMEGA= .3000E+02 M= 0 N= 1 XMN= .0000E+00  
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.10000000E+01 BMN = 0.00000000E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .3000E+02 M= 0 N= 2 XMN= .6205E+01  
CUTOFF RATIO FOR MODE= .2595E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.26166472E+01 BMN = 0.27171760E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .3000E+02 M= 0 N= 3 XMN= .1224E+02  
CUTUFF RATIO FOR MODE= .1316E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERRUR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.24929737E+01 BMN = 0.47091179E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

LARGEST PROPAGATING N FOR THIS M = 3  
ZFRSAPR Floating underflow PC= 3100

ZFRSAPR Floating underflow PC= 3146

MODE DATA

OMEGA= .3000E+02 M= 1 N= 1 XMN= .1371E+01  
CUTOFF RATIO FOR MODE= .1175E+02  
SUM OF BESSSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS  
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.15152306E+01 BMN = -0.42119467E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 1 N= 2 XMN= .6390E+01  
CUTOFF RATIO FOR MODE= .2520E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.19356938E+01 BMN = 0.32269858E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 1 N= 3 XMN= .1232E+02  
CUTOFF RATIO FOR MODE= .1307E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.43514410E+01 BMN = 0.30726765E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 2 N= 1 XMN= .2708E+01  
CUTOFF RATIO FOR MODE= .5946E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.20525722E+01 BMN = -0.42471320E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 2 N= 2 XMN= .6920E+01  
CUTOFF RATIO FOR MODE= .2327E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS  
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36560636E+01 BMN = 0.74837045E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 2 N= 3 XMN= .1258E+02  
CUTOFF RATIO FOR MODE= .1280E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.44592966E+01 BMN = -0.29055613E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 3 N= 1 XMN= .3987E+01  
CUTOFF RATIO FOR MODE= .4039E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.26023450E+01 BMN = -0.32589376E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 3 N= 2 XMN= .7747E+01  
CUTOFF RATIO FOR MODE= .2079E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.35705322E+01 BMN = -0.89511162E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 3 N= 3 XMN= .1301E+02  
CUTOFF RATIO FOR MODE= .1238E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS  
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.18754669E+00 BMN = 0.53089864E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -3 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 4 N= 1 XMN= .5200E+01  
CUTOFF RATIO FOR MODE= .3097E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.31336392E+01 BMN = -0.20930877E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -4 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 4 N= 2 XMN= .8798E+01  
CUTOFF RATIO FOR MODE= .1830E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.33061669E+01 BMN = -0.15169850E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -4 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 4 N= 3 XMN= .1359E+02  
CUTOFF RATIO FOR MODE= .1185E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.34317489E+01 BMN = 0.40298049E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0

M= -4 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 5 N= 1 XMN= .6355E+01  
CUTOFF RATIO FOR MODE= .2534E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36182370E+01 BMN = -0.11930907E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 5 N= 2 XMN= .9995E+01  
CUTOFF RATIO FOR MODE= .1611E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.32789852E+01 BMN = -0.15982724E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 5 N= 3 XMN= .1432E+02  
CUTOFF RATIO FOR MODE= .1125E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.30087871E+01 BMN = 0.16051647E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 6 N= 1 XMN= .7473E+01  
CUTOFF RATIO FOR MODE= .2155E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.40542452E+01 BMN = -0.61590101E-01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 1 OMEGA= .3000E+02

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 6 N= 2 XMN= .1127E+02  
CUTOFF RATIO FOR MODE= .1429E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.34647685E+01 BMN = -0.14296053E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 6 N= 3 XMN= .1518E+02  
CUTOFF RATIO FOR MODE= .1061E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.51904865E+01 BMN = -0.42382837E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 7 N= 1 XMN= .8565E+01  
CUTOFF RATIO FOR MODE= .1880E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.44478450E+01 BMN = -0.30159084E-01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -7 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 7 N= 2 XMN= .1257E+02  
CUTOFF RATIO FOR MODE= .1281E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.37694693E+01 BMN = -0.11581721E+01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -7 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 8 N= 1 XMN= .9641E+01  
CUTOFF RATIO FOR MODE= .1670E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.48101954E+01 BMN = -0.14625833E-01  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -8 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 8 N= 2 XMN= .1386E+02  
CUTOFF RATIO FOR MODE= .1162E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.41235105E+01 BMN = -0.85984372E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -8 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .3000E+02 M= 9 N= 1 XMN= .1071E+02  
CUTOFF RATIO FOR MODE= .1504E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.51513706E+01 BMN = -0.65555876E-02  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -9 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 9 N= 2 XMN= .1512E+02  
CUTOFF RATIO FOR MODE= .1063E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.44743524E+01 BMN = -0.59372922E+00  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -9 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

(4)

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 10 N= 1 XMN= .1177E+02  
CUTOFF RATIO FOR MODE= .1368E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.54757875E+01 BMN = -0.30348101E-02  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -10 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 11 N= 1 XMN= .1283E+02  
CUTOFF RATIO FOR MODE= .1256E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.57877752E+01 BMN = -0.13177058E-02  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -11 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 12 N= 1 XMN= .1388E+02  
CUTOFF RATIO FOR MODE= .1160E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.60893310E+01 BMN = -0.63729882E-03  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -12 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 13 N= 1 XMN= .1493E+02  
CUTOFF RATIO FOR MODE= .1079E+01  
SUM OF BESSSEL FUNCTION ERROR CODES = 0  
ERRUR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.63824353E+01 BMN = -0.1813051E-03  
ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -13 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 14 N= 1 XMN= .1598E+02

CUTOFF RATIO FOR MODE= .1008E+01

SUM OF BESSSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.66676797E+01 BMN = -0.10550421E-03

ERROR CODE FOR BESSSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -14 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS OMEGA

PROBLEM COMPLETED

STOP

END OF EXECUTION

CPU TIME: 1:40.60 ELAPSED TIME: 8:6.24

EXIT.